

3. Circuit implementation of the transfer function

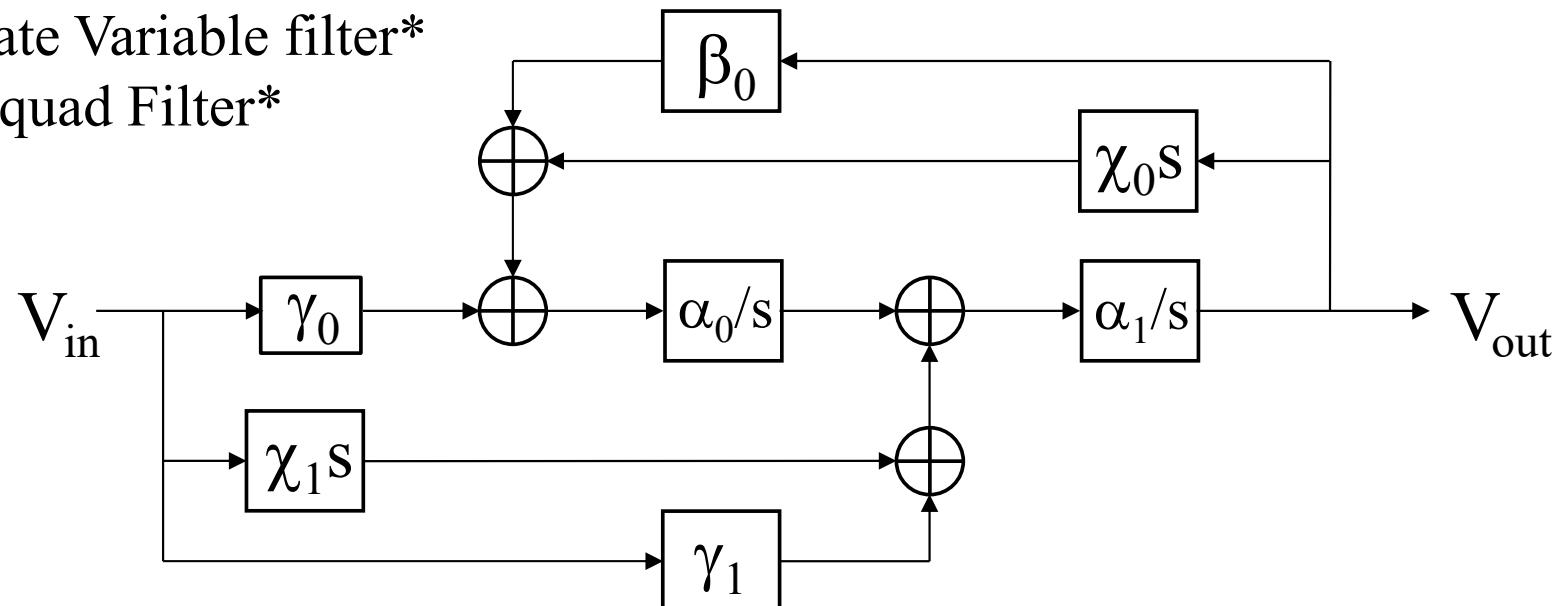
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Microelectronics Research Lab.
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3.1 Block diagram of continuous-time circuit

Block diagram design using linear operations

$$V_{\text{in}} \rightarrow \boxed{\frac{a \cdot s^2 + b \cdot s + c}{s^2 + d \cdot s + e}} \rightarrow V_{\text{out}}$$

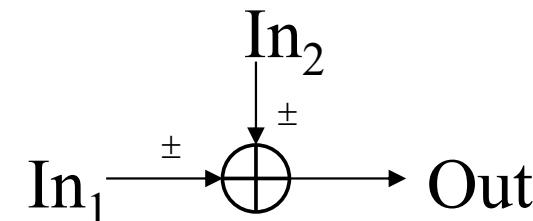
- Multiple Feedback Filter
- Sallen-Key filter
- State Variable filter*
- Biquad Filter*



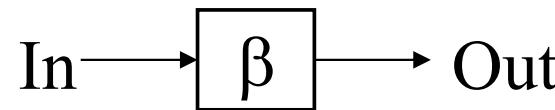
* The parameters of the transfer function can be set independently.

Linear operators for continuous-time circuit

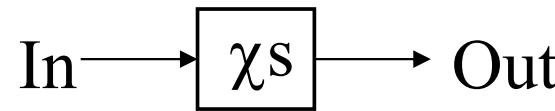
Adder and subtractor



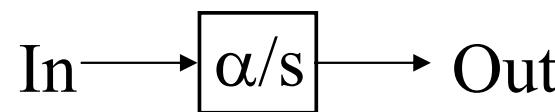
Constant multiplication



Differentiator



Integrator



The parameters β , χ , and α are the gain of an amplifier, a differentiator, and an integrator, respectively.

Block diagram of 1st-order LPF

$$V_{in} \rightarrow \boxed{\frac{b}{s+c}} \rightarrow V_{out}$$

Transfer function

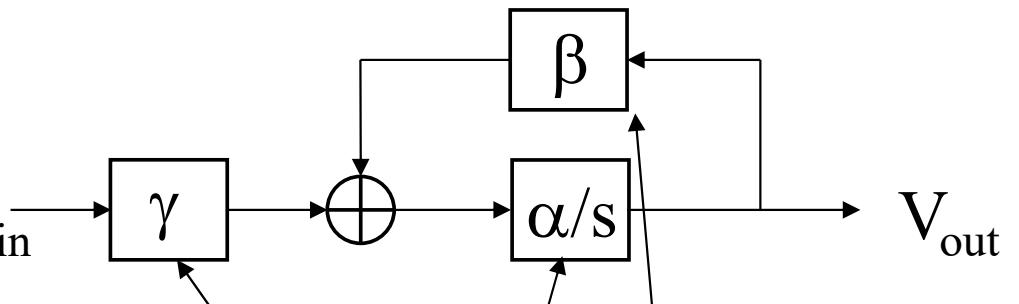
$$\frac{V_{out}}{V_{in}} = \frac{b}{s+c}$$

$$(s+c) \cdot V_{out} = b \cdot V_{in}$$

$$V_{out} = \frac{1}{s} (b \cdot V_{in} - c \cdot V_{out}) = \frac{\alpha}{s} \left(\frac{b}{\alpha} V_{in} - \frac{c}{\alpha} V_{out} \right) \equiv \frac{\alpha}{s} (\gamma \cdot V_{in} + \beta \cdot V_{out})$$

$$H(s) = \frac{V_{out}}{V_{in}} = \frac{b}{s+c} = \frac{\alpha \cdot \gamma}{s - \alpha \cdot \beta} \quad \left\{ \begin{array}{l} b = \alpha \cdot \gamma \\ c = -\alpha \cdot \beta \end{array} \right.$$

NOTE: A feedback of a constant introduces a constant term in a denominator.



Block diagram of transfer function

Block diagram of 1st-order HPF

$$V_{in} \rightarrow \boxed{\frac{a \cdot s}{s + c}} \rightarrow V_{out}$$

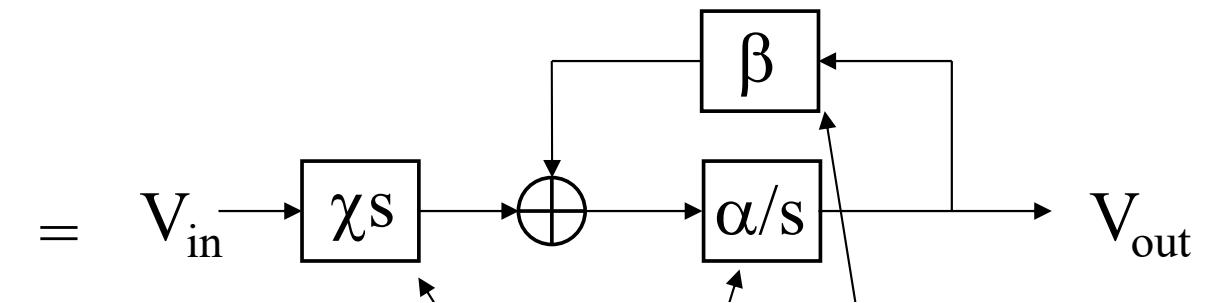
Transfer function

$$\frac{V_{out}}{V_{in}} = \frac{a \cdot s}{s + c}$$

$$(s + c) \cdot V_{out} = a \cdot s \cdot V_{in}$$

$$V_{out} = \frac{1}{s} (a \cdot s \cdot V_{in} - c \cdot V_{out}) = \frac{\alpha}{s} \left(\frac{a}{\alpha} s \cdot V_{in} - \frac{c}{\alpha} V_{out} \right) \equiv \frac{\alpha}{s} (\chi \cdot s \cdot V_{in} + \beta \cdot V_{out})$$

$$H(s) = \frac{V_{out}}{V_{in}} = \frac{a \cdot s}{s + c} = \frac{\alpha \cdot \chi \cdot s}{s - \alpha \cdot \beta}$$



Block diagram of transfer function

$$\begin{aligned}
 & \text{Left side: } H(s) = \frac{V_{out}}{V_{in}} = \frac{a \cdot s}{s + c} = \frac{\alpha \cdot \chi \cdot s}{s - \alpha \cdot \beta} \\
 & \text{Right side: } \frac{\alpha}{s} (\chi \cdot s \cdot V_{in} + \beta \cdot V_{out}) \\
 & \text{Equating coefficients: }
 \begin{cases}
 a = \alpha \cdot \chi \\
 c = -\alpha \cdot \beta
 \end{cases}
 \end{aligned}$$

Block diagram of 1st-order transfer function

$$V_{\text{in}} \rightarrow \boxed{\frac{a \cdot s + b}{s + c}} \rightarrow V_{\text{out}} =$$

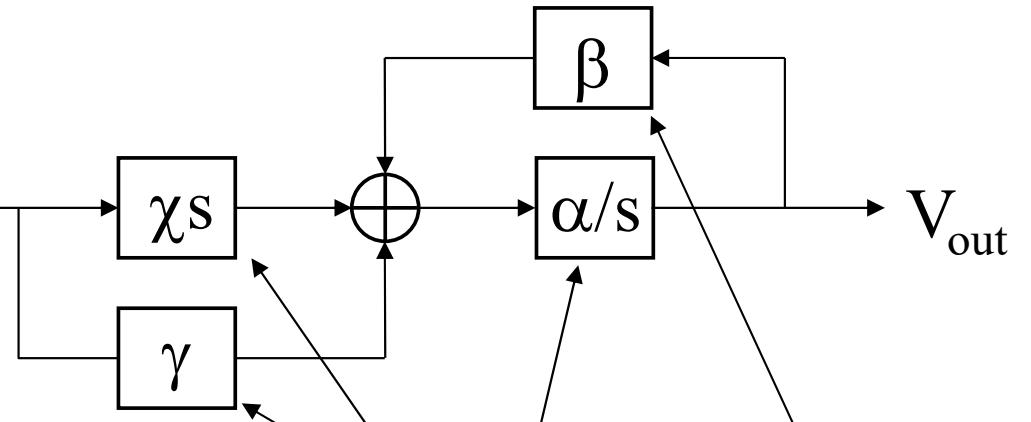
Transfer function

$$\frac{V_{\text{out}}}{V_{\text{in}}} = \frac{a \cdot s + b}{s + c}$$

$$(s + c) \cdot V_{\text{out}} = (a \cdot s + b) \cdot V_{\text{in}}$$

$$V_{\text{out}} = \frac{1}{s} (a \cdot s \cdot V_{\text{in}} + b \cdot V_{\text{in}} - c \cdot V_{\text{out}}) = \frac{\alpha}{s} \left(\frac{a}{\alpha} s \cdot V_{\text{in}} + \frac{b}{\alpha} V_{\text{in}} - \frac{c}{\alpha} V_{\text{out}} \right) \equiv \frac{\alpha}{s} (\chi \cdot s \cdot V_{\text{in}} + \gamma \cdot V_{\text{in}} + \beta \cdot V_{\text{out}})$$

$$H(s) = \frac{V_{\text{out}}}{V_{\text{in}}} = \frac{a \cdot s + b}{s + c} = \frac{\alpha \cdot \chi \cdot s + \alpha \cdot \gamma}{s - \alpha \cdot \beta}$$



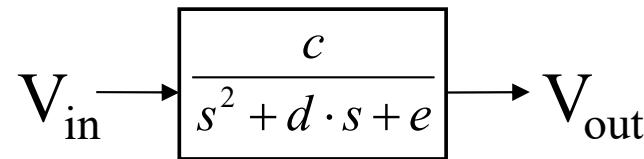
Block diagram of transfer function

$$\left\{ \begin{array}{l} a = \alpha \cdot \chi \\ b = \alpha \cdot \gamma \\ c = -\alpha \cdot \beta \end{array} \right.$$

Block diagram of 2nd-order LPF 1

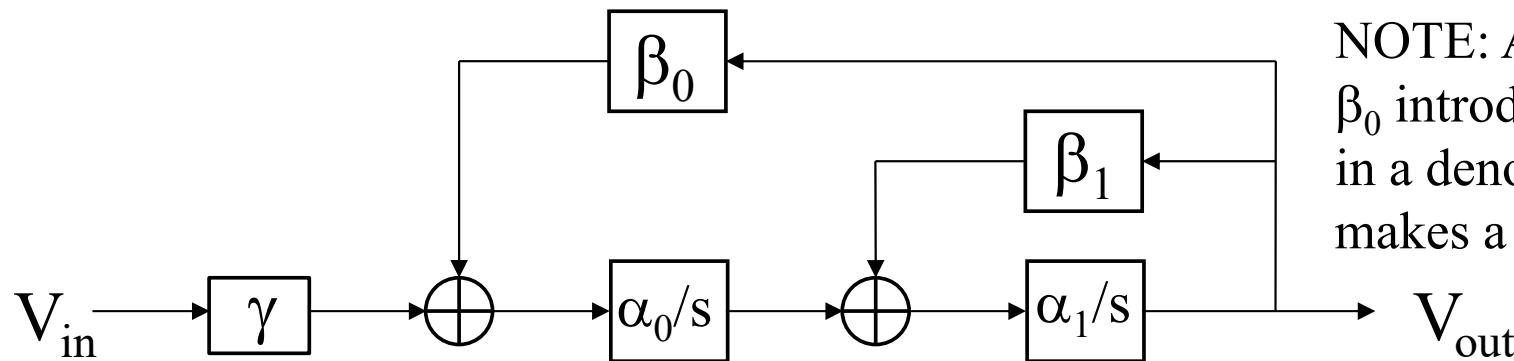
$$\frac{V_{out}}{V_{in}} = \frac{c}{s^2 + d \cdot s + e}$$

$$(s^2 + d \cdot s + e) \cdot V_{out} = c \cdot V_{in}$$



$$V_{out} = \frac{1}{s^2} (c \cdot V_{in} - d \cdot s \cdot V_{out} - e \cdot V_{out}) = \frac{1}{s} \left\{ \frac{1}{s} (c \cdot V_{in} - e \cdot V_{out}) - d \cdot V_{out} \right\}$$

$$= \frac{\alpha_1}{s} \left\{ \frac{\alpha_0}{s} \left(\frac{c}{\alpha_1 \alpha_0} V_{in} - \frac{e}{\alpha_1 \alpha_0} V_{out} \right) - \frac{d}{\alpha_1} V_{out} \right\} \equiv \frac{\alpha_1}{s} \left\{ \frac{\alpha_0}{s} (\gamma \cdot V_{in} + \beta_0 \cdot V_{out}) + \beta_1 \cdot V_{out} \right\}$$



NOTE: A feedback element β_0 introduces a constant term in a denominator, and β_1 makes a design flexibility.

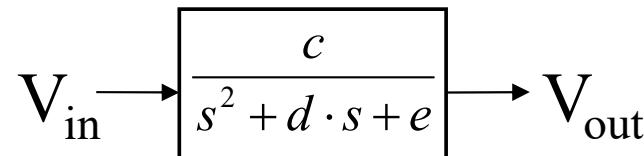
$$H(s) = \frac{V_{out}}{V_{in}} = \frac{c}{s^2 + d \cdot s + e} = \frac{\alpha_0 \cdot \alpha_1 \cdot \gamma}{s^2 - \alpha_1 \cdot \beta_1 \cdot s - \alpha_0 \cdot \alpha_1 \cdot \beta_0}$$

$$\begin{cases} c = \alpha_0 \cdot \alpha_1 \cdot \gamma \\ d = -\alpha_1 \cdot \beta_1 \\ e = -\alpha_0 \cdot \alpha_1 \cdot \beta_0 \end{cases}$$

Block diagram of 2nd-order LPF 2

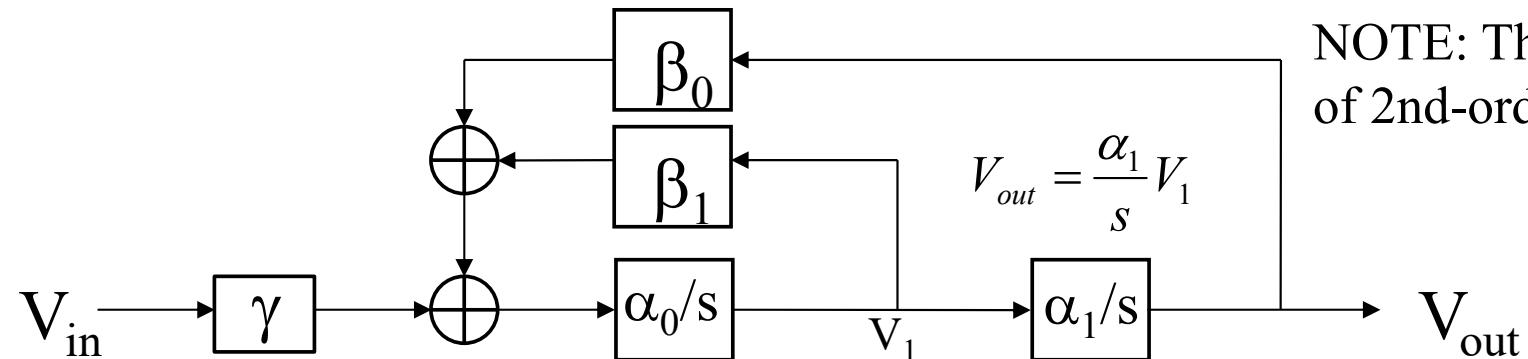
$$\frac{V_{out}}{V_{in}} = \frac{c}{s^2 + d \cdot s + e}$$

$$(s^2 + d \cdot s + e) \cdot V_{out} = c \cdot V_{in}$$



$$V_{out} = \frac{1}{s^2} (c \cdot V_{in} - d \cdot s \cdot V_{out} - e \cdot V_{out}) = \frac{\alpha_1}{s} \frac{\alpha_0}{s} \left(\frac{c}{\alpha_1 \alpha_0} \cdot V_{in} - \frac{d}{\alpha_0} \frac{s}{\alpha_1} V_{out} - \frac{e}{\alpha_1 \alpha_0} V_{out} \right)$$

$$= \frac{\alpha_1}{s} \frac{\alpha_0}{s} \left(\frac{c}{\alpha_1 \alpha_0} \cdot V_{in} - \frac{d}{\alpha_0} V_1 - \frac{e}{\alpha_1 \alpha_0} V_{out} \right) \equiv \frac{\alpha_1}{s} \frac{\alpha_0}{s} (\gamma \cdot V_{in} + \beta_1 \cdot V_1 + \beta_0 \cdot V_{out})$$



NOTE: This is another solution of 2nd-order LPF.

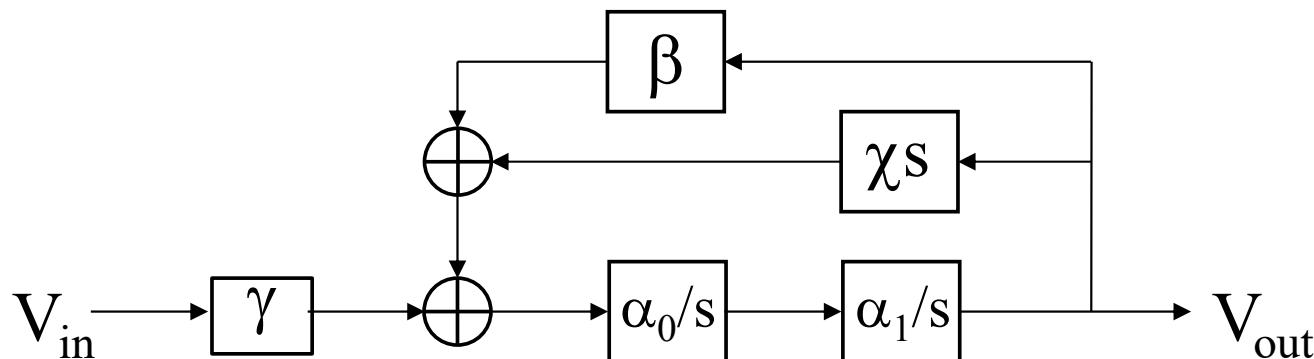
$$H(s) = \frac{V_{out}}{V_{in}} = \frac{c}{s^2 + d \cdot s + e} = \frac{\alpha_0 \cdot \alpha_1 \cdot \gamma}{s^2 - \alpha_1 \cdot \beta_1 \cdot s - \alpha_0 \cdot \alpha_1 \cdot \beta_0}$$

$$\left\{ \begin{array}{l} c = \alpha_0 \cdot \alpha_1 \cdot \gamma \\ d = -\alpha_0 \cdot \beta_1 \\ e = -\alpha_0 \cdot \alpha_1 \cdot \beta_0 \end{array} \right.$$

Block diagram of 2nd-order LPF 3

$$\begin{aligned}
 V_{out} &= \frac{1}{s^2}(c \cdot V_{in} - d \cdot s \cdot V_{out} - e \cdot V_{out}) \\
 &= \frac{\alpha_0}{s} \frac{\alpha_1}{s} \left(\frac{c}{\alpha_0 \alpha_1} V_{in} - \frac{d}{\alpha_0 \alpha_1} s \cdot V_{out} - \frac{e}{\alpha_0 \alpha_1} V_{out} \right) \\
 &\equiv \frac{\alpha_0}{s} \frac{\alpha_1}{s} (\gamma \cdot V_{in} + \chi \cdot s \cdot V_{out} + \beta \cdot V_{out})
 \end{aligned}$$

$$V_{in} \rightarrow \boxed{\frac{c}{s^2 + d \cdot s + e}} \rightarrow V_{out}$$



$$H(s) = \frac{V_{out}}{V_{in}} = \frac{c}{s^2 + d \cdot s + e} = \frac{\alpha_0 \cdot \alpha_1 \cdot \gamma}{s^2 - \alpha_0 \cdot \alpha_1 \cdot \chi \cdot s - \alpha_0 \cdot \alpha_1 \cdot \beta} \quad \leftarrow \quad \begin{cases} c = \alpha_0 \cdot \alpha_1 \cdot \gamma \\ d = -\alpha_0 \cdot \alpha_1 \cdot \chi \\ e = -\alpha_0 \cdot \alpha_1 \cdot \beta \end{cases}$$

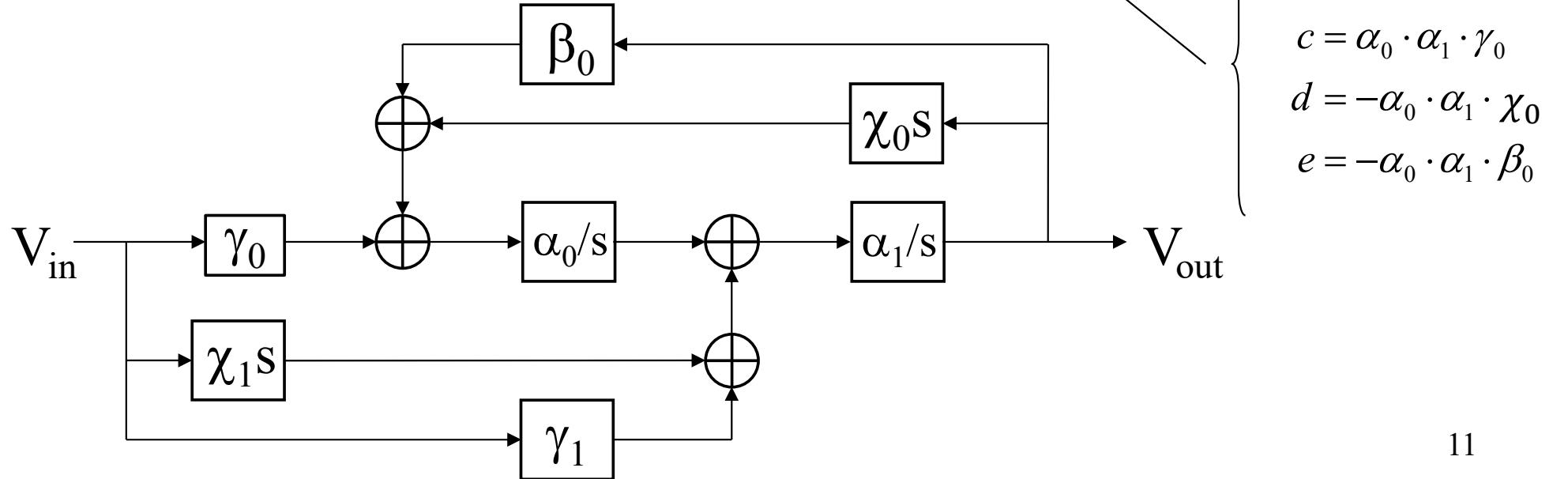
Block diagram of 2nd-order transfer function

$$\frac{V_{out}}{V_{in}} = \frac{a \cdot s^2 + b \cdot s + c}{s^2 + d \cdot s + e}$$

$$V_{out} = \frac{1}{s^2} (a \cdot s^2 \cdot V_{in} + b \cdot s \cdot V_{in} + c \cdot V_{in}) + \frac{1}{s^2} (-d \cdot s \cdot V_{out} - e \cdot V_{out})$$

$$= \frac{\alpha_0}{s} \frac{\alpha_1}{s} \frac{c}{\alpha_0 \alpha_1} \cdot V_{in} + \frac{\alpha_1}{s} \left(\frac{a}{\alpha_1} \cdot s \cdot V_{in} + \frac{b}{\alpha_1} \cdot V_{in} \right) + \frac{\alpha_0}{s} \frac{\alpha_1}{s} \left(-\frac{d}{\alpha_0 \alpha_1} \cdot s \cdot V_{out} - \frac{e}{\alpha_0 \alpha_1} \cdot V_{out} \right)$$

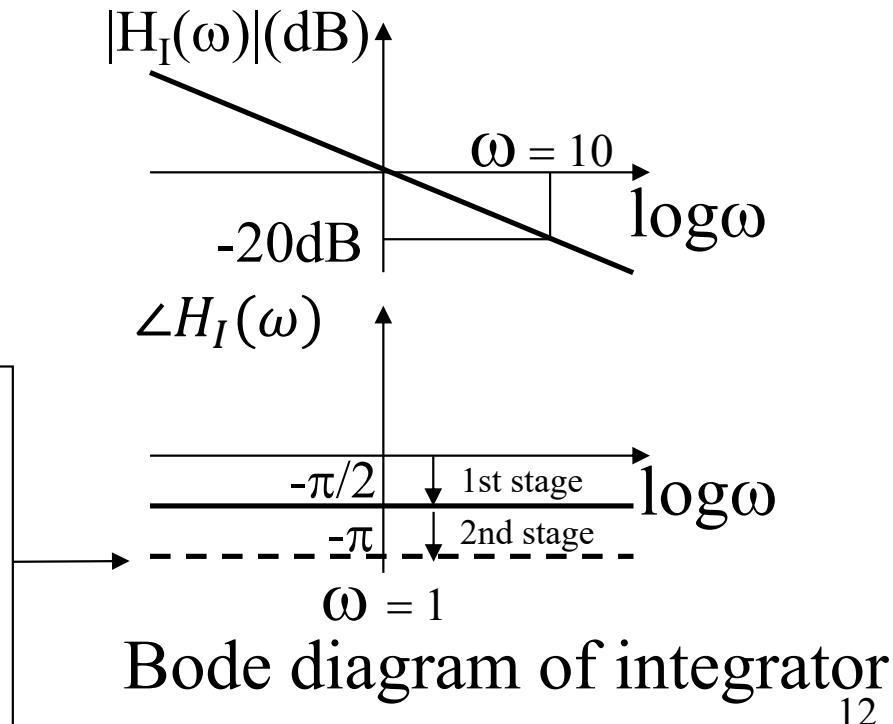
$$\equiv \frac{\alpha_0}{s} \frac{\alpha_1}{s} \gamma_0 \cdot V_{in} + \frac{\alpha_1}{s} (\chi_1 \cdot s \cdot V_{in} + \gamma_1 \cdot V_{in}) + \frac{\alpha_0}{s} \frac{\alpha_1}{s} (\chi_0 \cdot s \cdot V_{out} + \beta_0 \cdot V_{out})$$



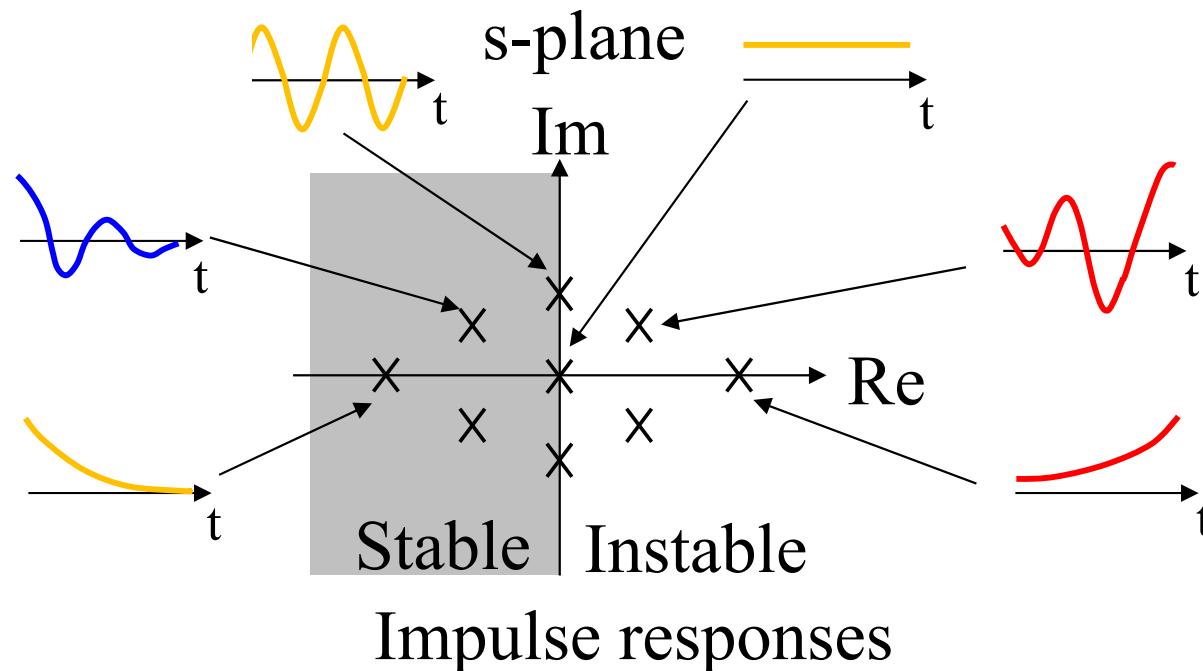
Stability of higher order transfer function

- A 2-stage-cascade connection of the integrators or differentiators can cause instability of the circuit with the feedback loop, because of the phase rotation $> \pi$. In the worst case, the circuit unexpectedly oscillates.

The feedback loop with the phase shift $> \pi$ causes the negative feedback (NFB) or positive feedback (PFB).



Stability of transfer functions



You can simply check the stability of the circuit with the pole arrangement of the transfer function. The poles on the imaginary axis and right half plane cause the instability or the metastability of the circuit.

3.2 Block diagram of discrete-time circuit

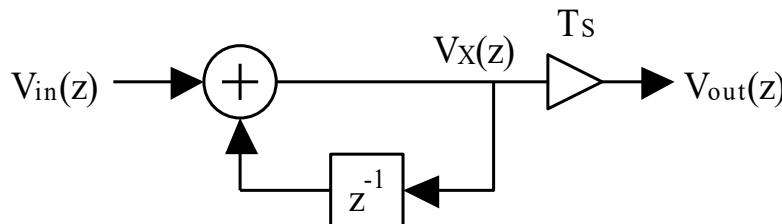
Integrator and differentiator (1)

Integrator by BET

$$V_{out}(z) = \frac{T_S}{1 - z^{-1}} V_{in}(z)$$

Differentiator by BET

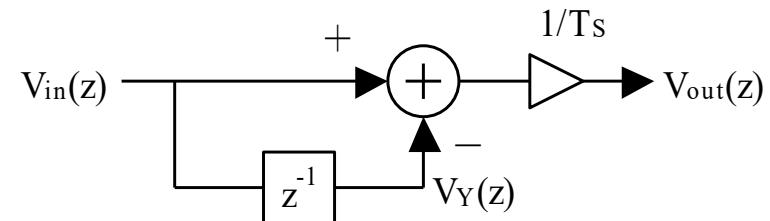
$$V_{out}(z) = \frac{1 - z^{-1}}{T_S} V_{in}(z)$$



$$V_X(z) = V_{in}(z) + z^{-1}V_X(z)$$

$$V_X(z) = \frac{V_{in}(z)}{1 - z^{-1}}$$

$$V_{out}(z) = T_S \cdot V_X(z) = \frac{T_S}{1 - z^{-1}} V_{in}(z)$$



$$V_Y(z) = z^{-1}V_{in}(z)$$

$$V_{out}(z) = \frac{1}{T_S} \{-z^{-1}V_{in}(z) + V_{in}(z)\}$$

$$= \frac{1 - z^{-1}}{T_S} V_{in}(z)$$

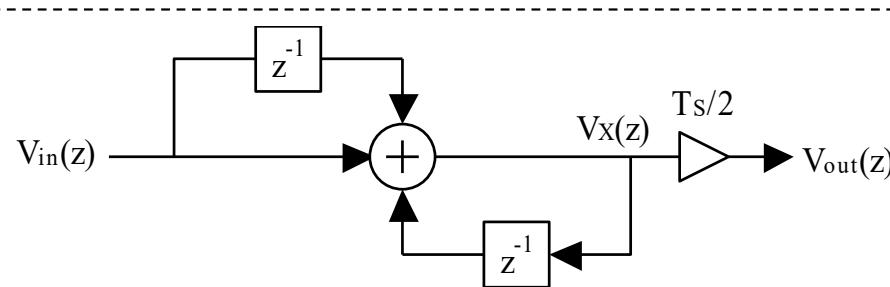
Integrator and differentiator (2)

Integrator by bilinear transform

$$V_{out}(z) = \frac{T_S}{2} \frac{1+z^{-1}}{1-z^{-1}} V_{in}(z)$$

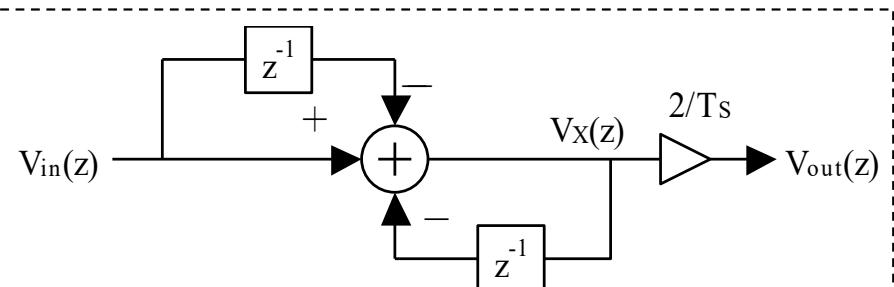
Differentiator by bilinear transform

$$V_{out}(z) = \frac{2}{T_S} \frac{1-z^{-1}}{1+z^{-1}} V_{in}(z)$$



$$\begin{aligned} V_X(z) &= (1+z^{-1})V_{in}(z) + z^{-1}V_X(z) \\ (1-z^{-1})V_X(z) &= (1+z^{-1})V_{in}(z) \end{aligned}$$

$$V_{out}(z) = \frac{T_S}{2} V_X(z) = \frac{T_S}{2} \frac{1+z^{-1}}{1-z^{-1}} V_{in}(z)$$



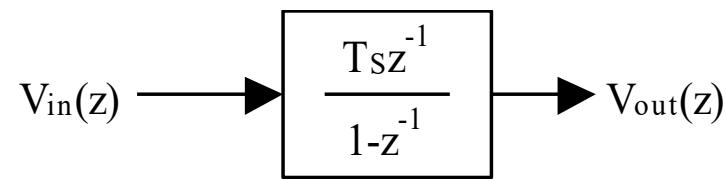
$$\begin{aligned} V_X(z) &= (1-z^{-1})V_{in}(z) - z^{-1}V_X(z) \\ (1+z^{-1})V_X(z) &= (1-z^{-1})V_{in}(z) \end{aligned}$$

$$V_{out}(z) = \frac{2}{T_S} V_X(z) = \frac{2}{T_S} \frac{1-z^{-1}}{1+z^{-1}} V_{in}(z)$$

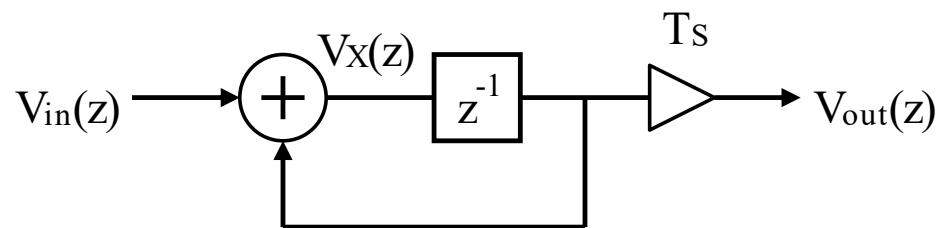
Integrator

Integrator by FET

$$V_{out}(z) = \frac{T_s \cdot z^{-1}}{1 - z^{-1}} V_{in}(z)$$



The FET integrator is equivalent to the BET integrator + the delay element of T_s .



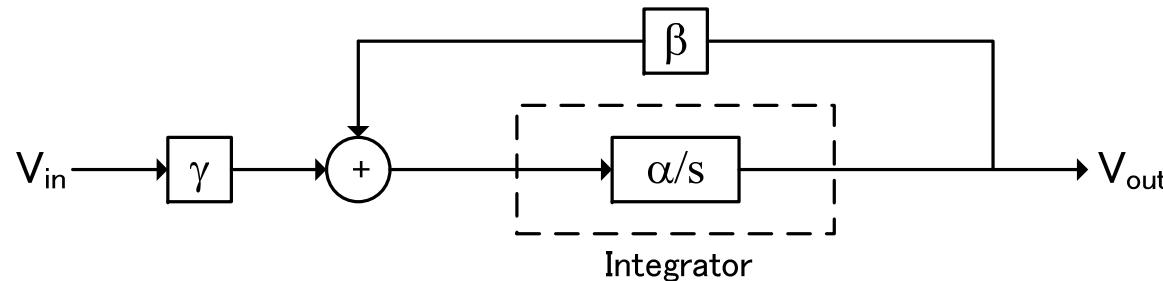
NOTE: The integrator and delaying integrator show the same characteristic except for delay time. The delaying integrator **does not output the hazard** generated by the adder.

Block diagram of variable s and z

Examples of 1st-order LPF

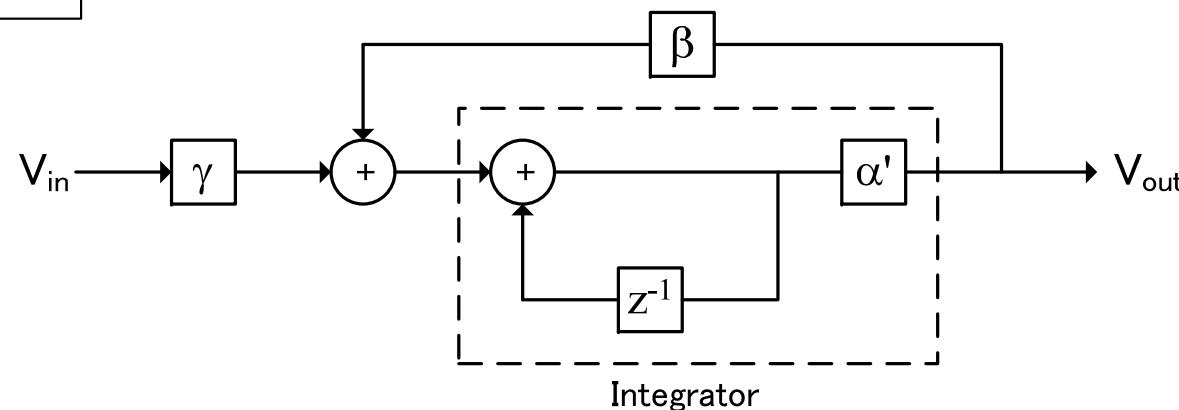
variable s

Continuous-time analog circuits

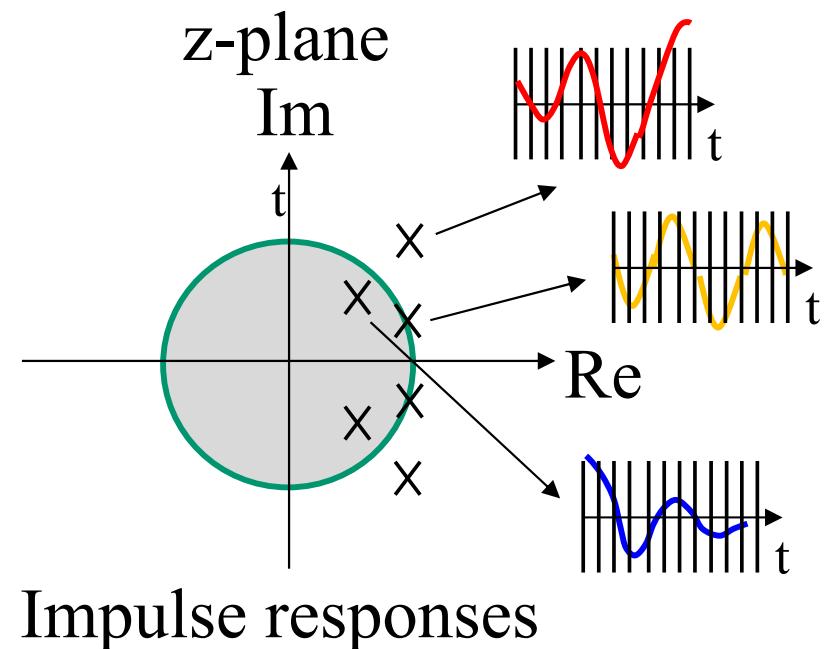
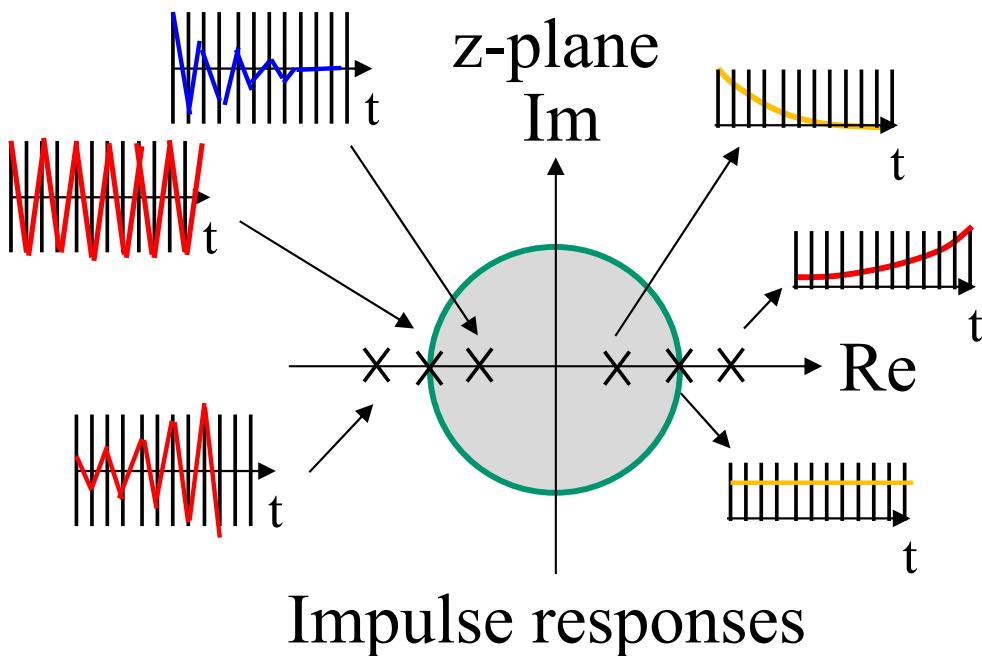


variable z

Discrete-time analog circuits and digital circuits



Stability of transfer functions



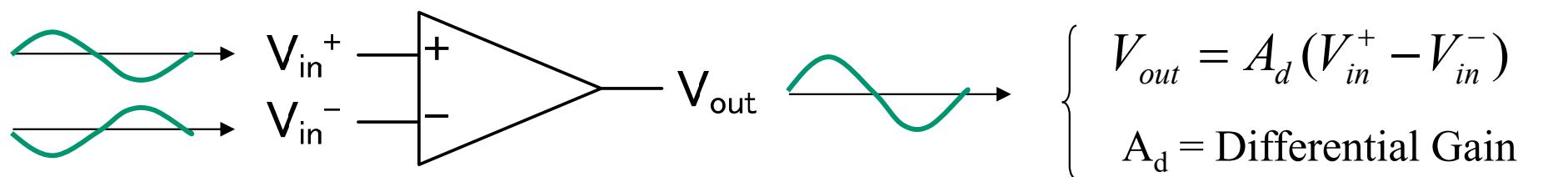
You can simply check the stability of the circuit with the pole arrangement of the transfer function. **The poles on the circumference or in the exterior of the unit circle cause the instability or the metastability of the circuit.**

3.3 Continuous-time analog implementation

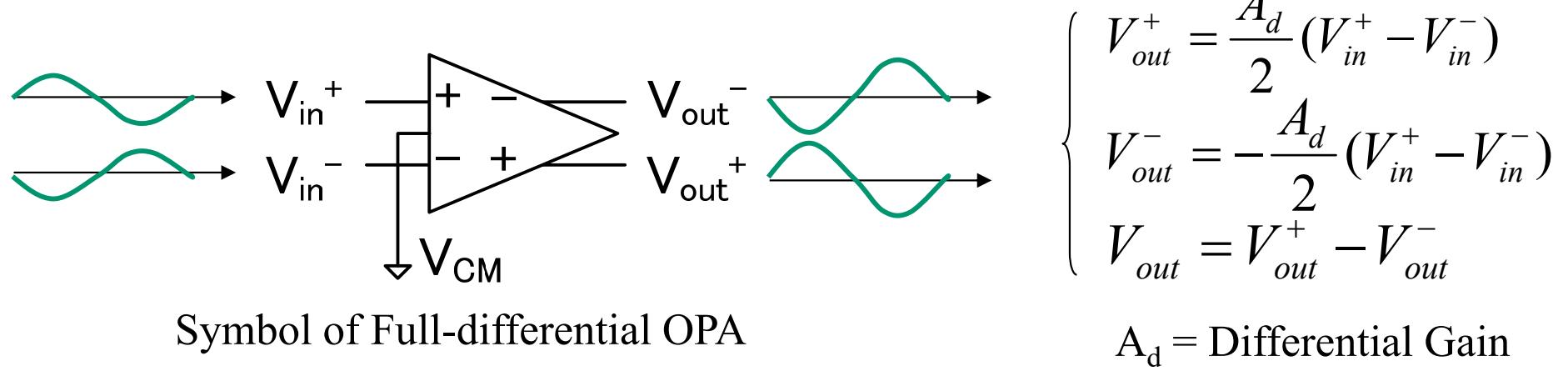
Implementation methods of analog circuits

| Signal | Circuitry | Components | Features |
|-----------------|--------------------|-----------------------------|---------------------------------------|
| Continuous time | RC | R, C, OPA | High precision, low power consumption |
| | gm-C | C, OTA | High speed, low power consumption |
| Discrete time | Switched capacitor | C, CMOS-switch, OPA | Very high precision |
| | Switched Current | Current mirror, CMOS-switch | Very high speed |

2 types of OPA

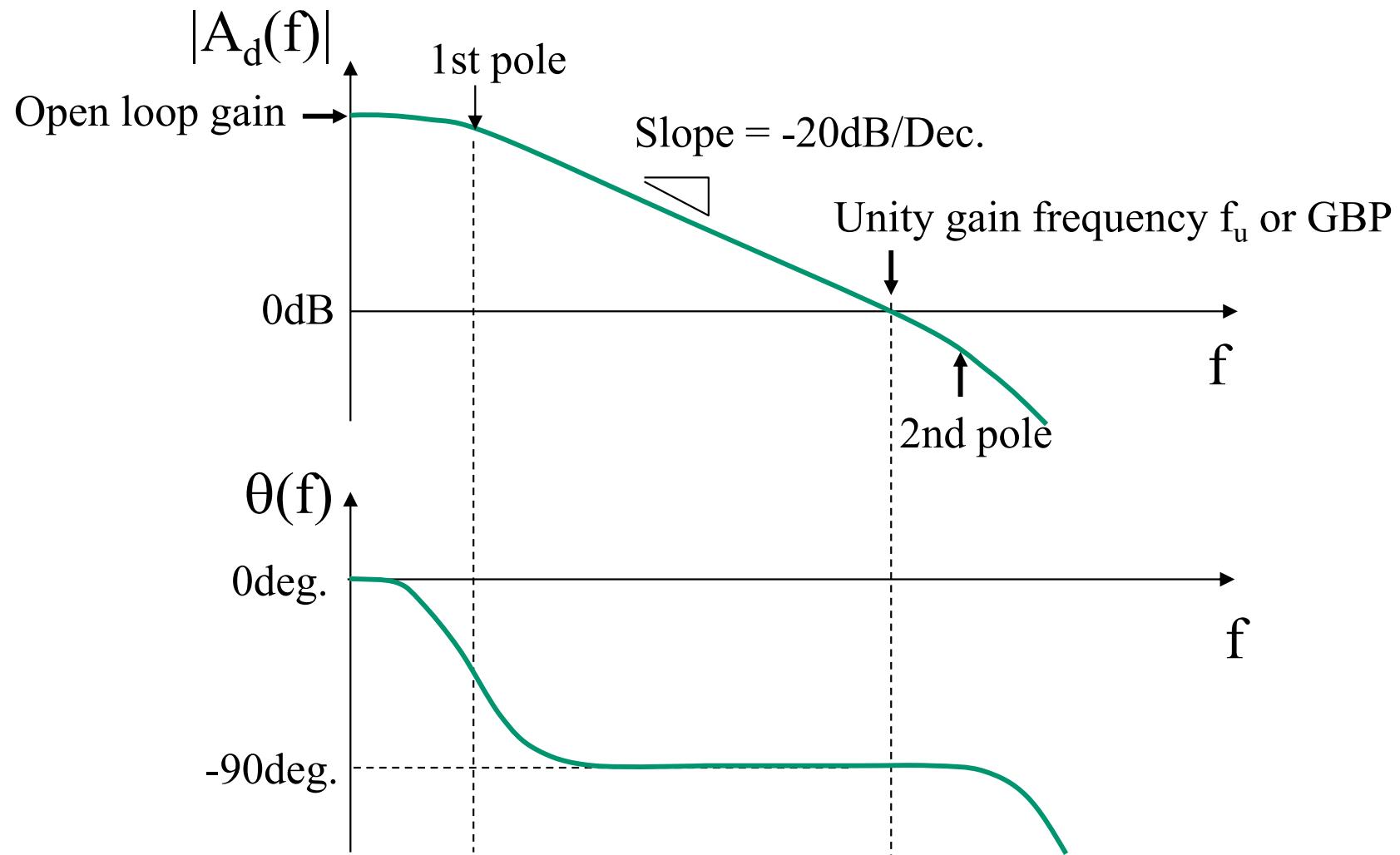


Symbol of Single-end OPA



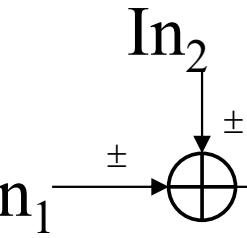
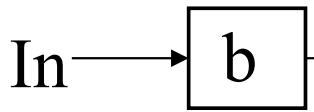
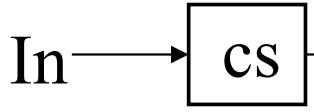
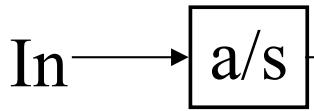
Symbol of Full-differential OPA

AC characteristic of OPA



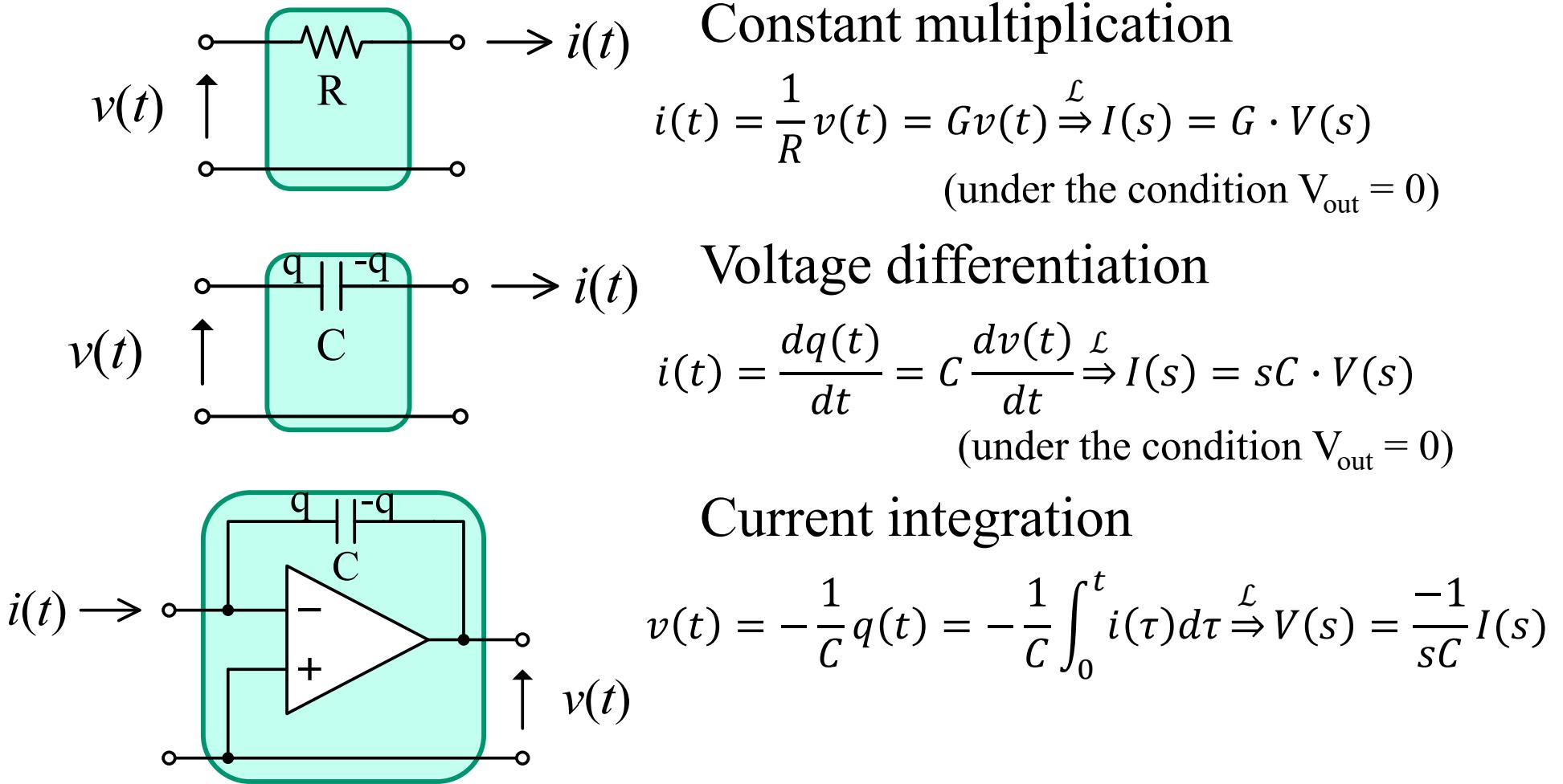
Linear operators

Linear operation elements in the analog circuits

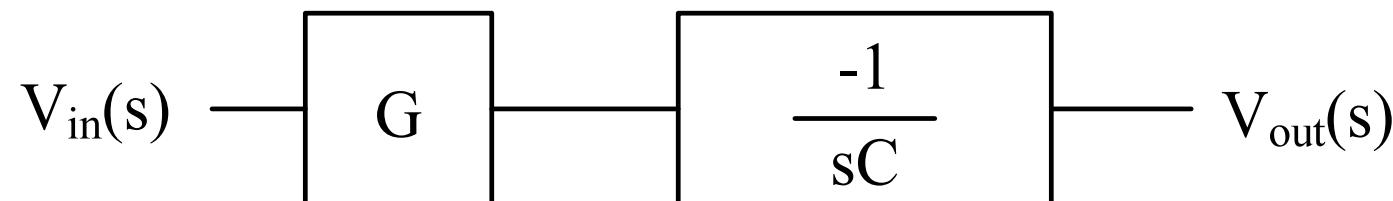
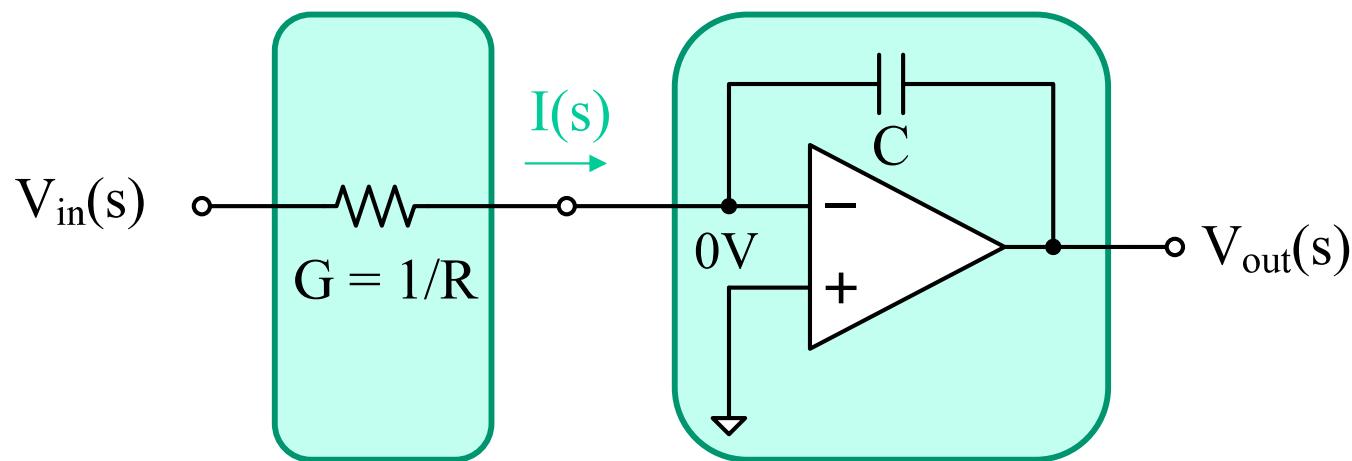
| Operation | Symbol | (Typical implementation) |
|--------------------------|--|--------------------------|
| Addition and subtraction |  | (Current summing) |
| Constant factor |  | (Resistor) |
| Derivation |  | (Capacitor) |
| Integral |  | (OPA or OTA) |

a, b, c : circuit constants

Continuous-time analog operators

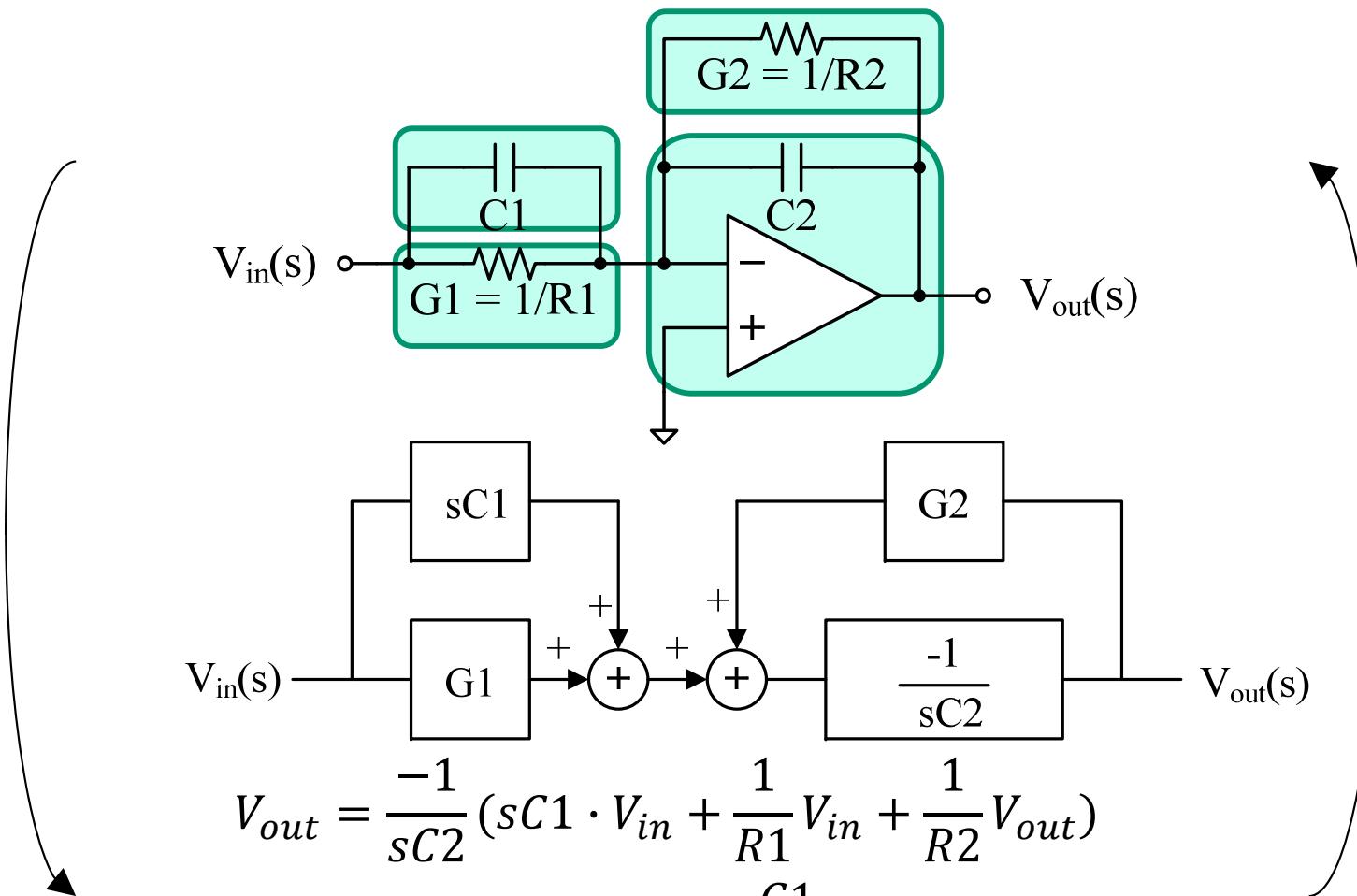


Continuous-time analog integrator (CAI)



Transfer function of CAI: $H(s) = \frac{V_{out}(s)}{V_{in}(s)} = -\frac{\frac{G}{sC}}{s} = -\frac{G}{s^2C}$

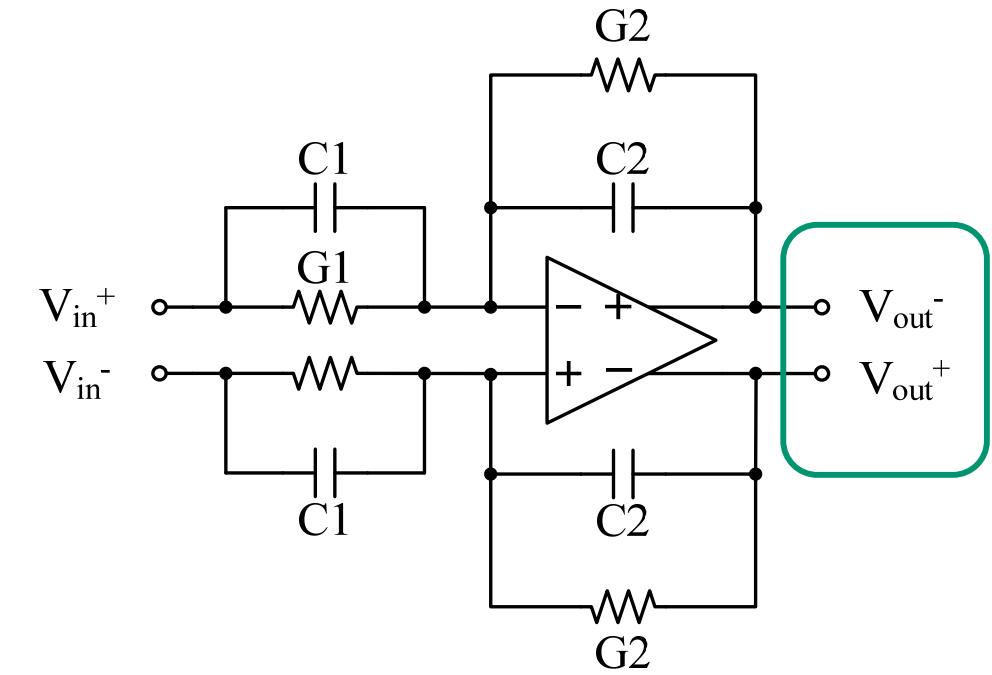
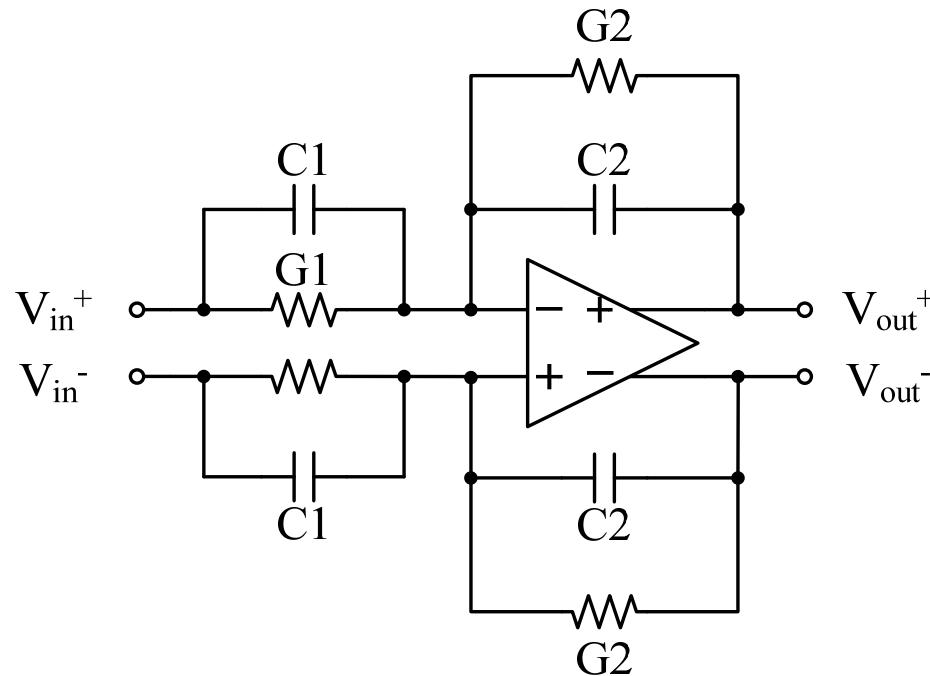
Implementation example 1



$$V_{out} = \frac{-1}{sC_2} (sC_1 \cdot V_{in} + \frac{1}{R_1} V_{in} + \frac{1}{R_2} V_{out})$$

$$H(s) = \frac{V_{out}}{V_{in}} = -\frac{C_1 s + \frac{G_1}{C_1}}{C_2 s + \frac{G_2}{C_2}} = a \frac{s + b}{s + c}$$

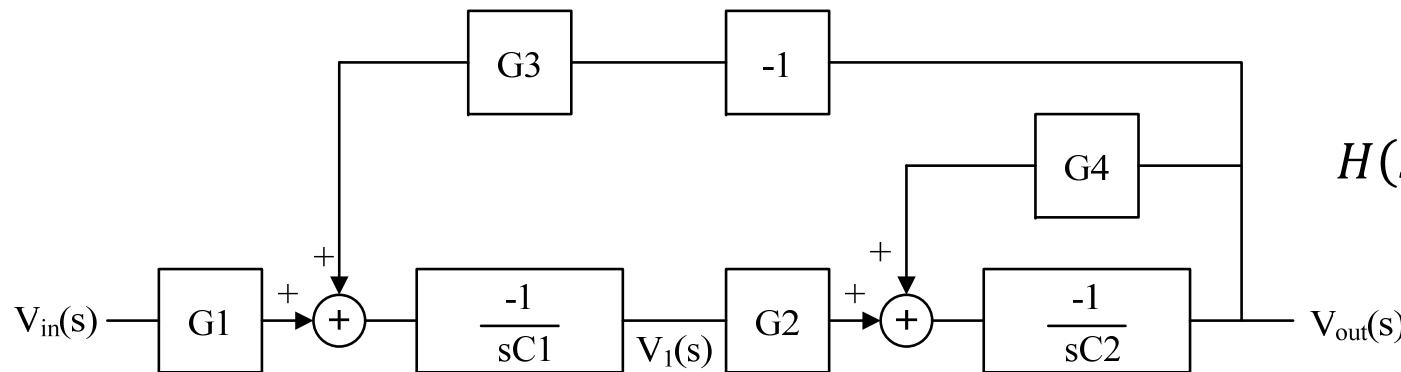
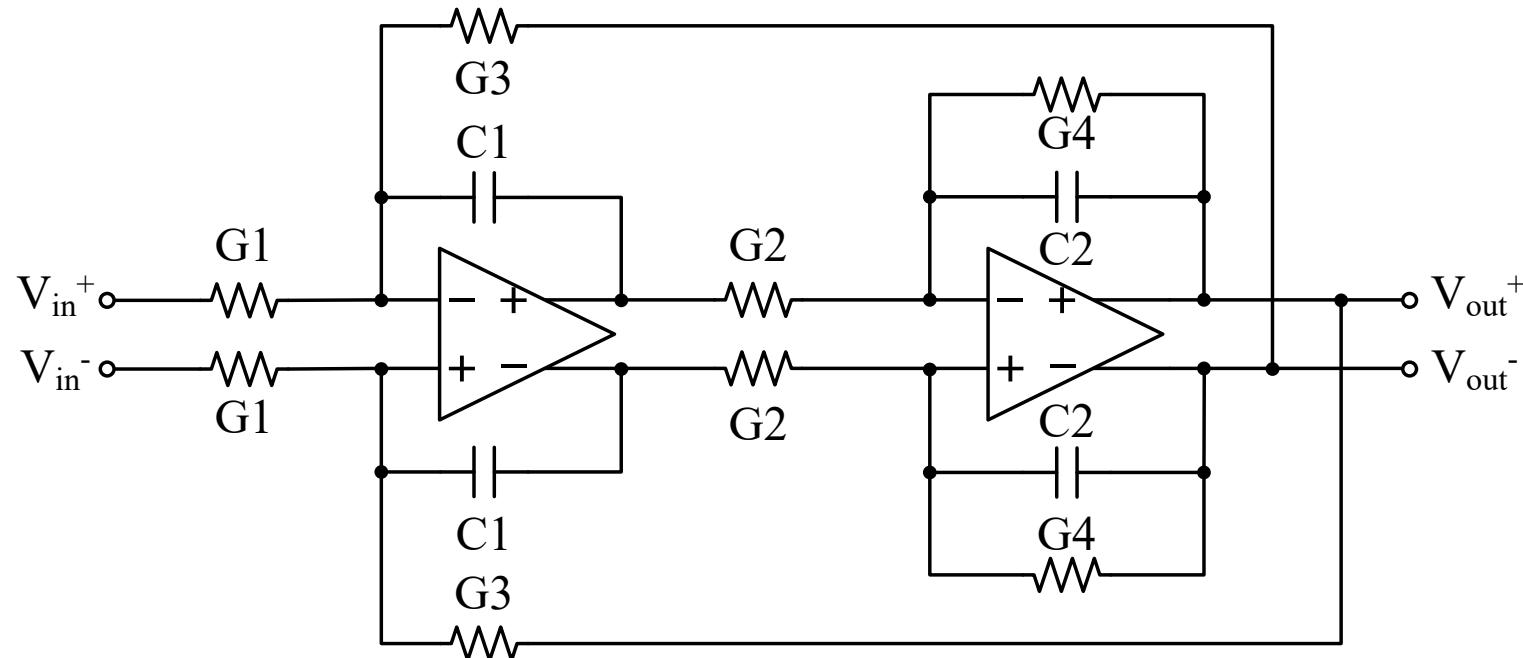
Full-differential implementation



$$H(s) = \frac{V_{out}}{V_{in}} = -\frac{C_1 s + \frac{G_1}{C_1}}{C_2 s + \frac{G_2}{C_2}}$$

$$H(s) = \frac{V_{out}}{V_{in}} = \frac{C_1 s + \frac{G_1}{C_1}}{C_2 s + \frac{G_2}{C_2}}$$

Implementation example 2



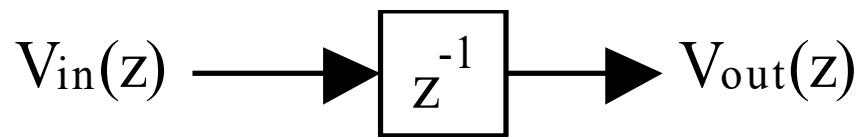
$$H(s) = \frac{\frac{G_1 G_2}{C_1 C_2}}{s^2 + \frac{G_4}{C_2} s + \frac{G_2 G_3}{C_1 C_2}}$$

3.4 Discrete-time analog implementation

Delay element

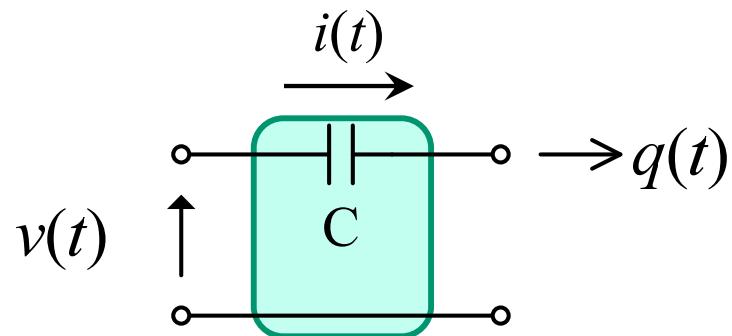
$$x_d(t - T_S) = x(t) \cdot \delta(t - T_S)$$

$$\begin{aligned} \int_0^\infty x_d(t - T_S) \cdot e^{-st} dt &= \int_0^\infty x(t) \cdot \delta(t - T_S) \cdot e^{-st} dt \\ &= x(T_S) e^{-sT_S} = x(T_S) \cdot z^{-1} \end{aligned}$$



$v(t) \rightarrow$ Time shift for 1-cycle $\rightarrow v(t - T_S)$

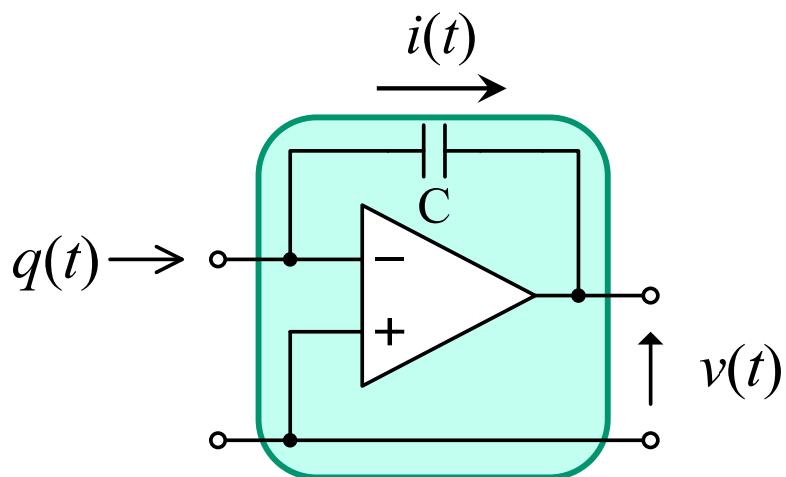
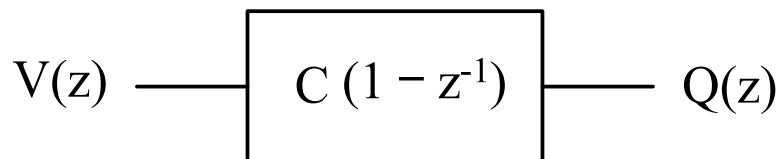
Discrete-time analog operators 1



Voltage derivation

$$I(s) = sC \cdot V(s) \xrightarrow{BET} I(z) = C(1 - z^{-1}) \frac{1}{T_S} V(z)$$

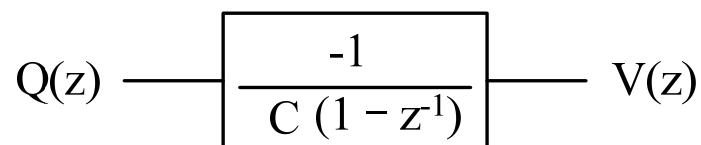
$$Q(z) = I(z)T_S = C(1 - z^{-1})V(z)$$



Charge integration

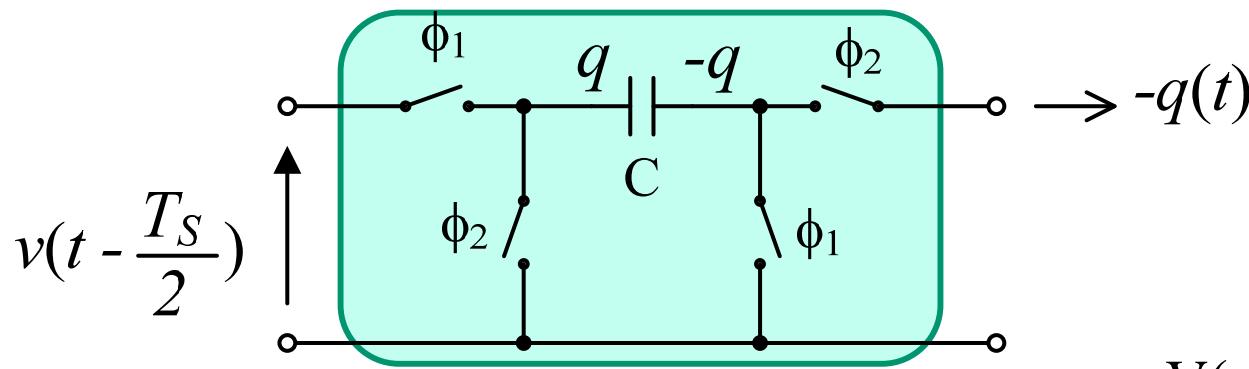
$$V(s) = \frac{-1}{sC} I(s) \xrightarrow{BET} V(z) = \frac{-1}{C} \frac{1}{1 - z^{-1}} I(z) T_S$$

$$V(z) = \frac{-1}{C} \frac{1}{1 - z^{-1}} Q(z)$$



Discrete-time analog operators 2

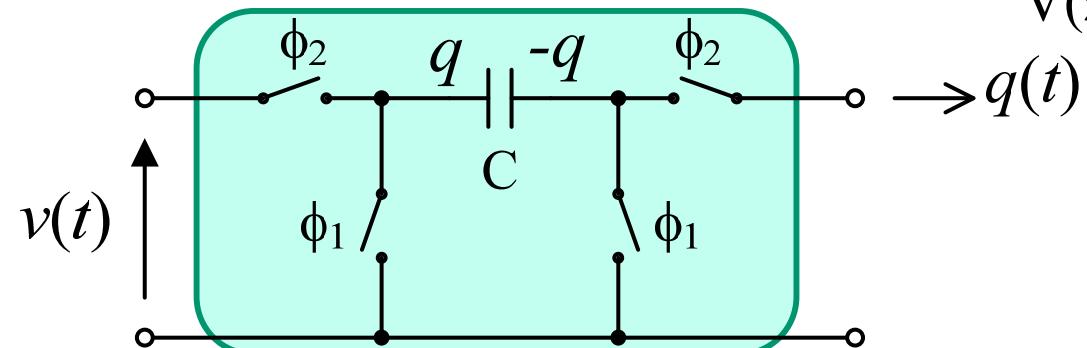
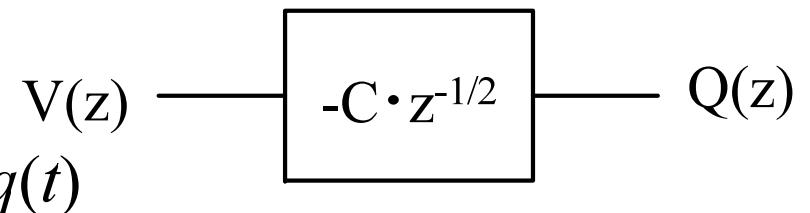
Constant multiplication (Switched capacitor)



(under the condition $V_{out} = 0$)

$$-q(t) = C \cdot v \left(t - \frac{T_S}{2} \right)$$

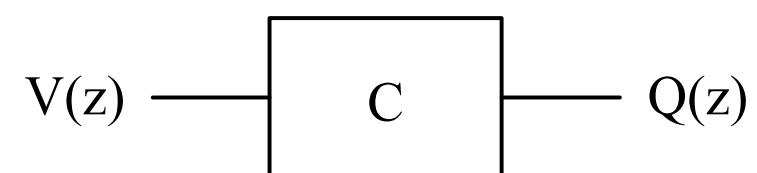
$$\stackrel{z}{\Rightarrow} -Q(z) = C \cdot V(z) z^{-\frac{1}{2}}$$



(under the condition $V_{out} = 0$)

$$q(t) = C \cdot v(t)$$

$$\stackrel{z}{\Rightarrow} Q(z) = C \cdot V(z)$$

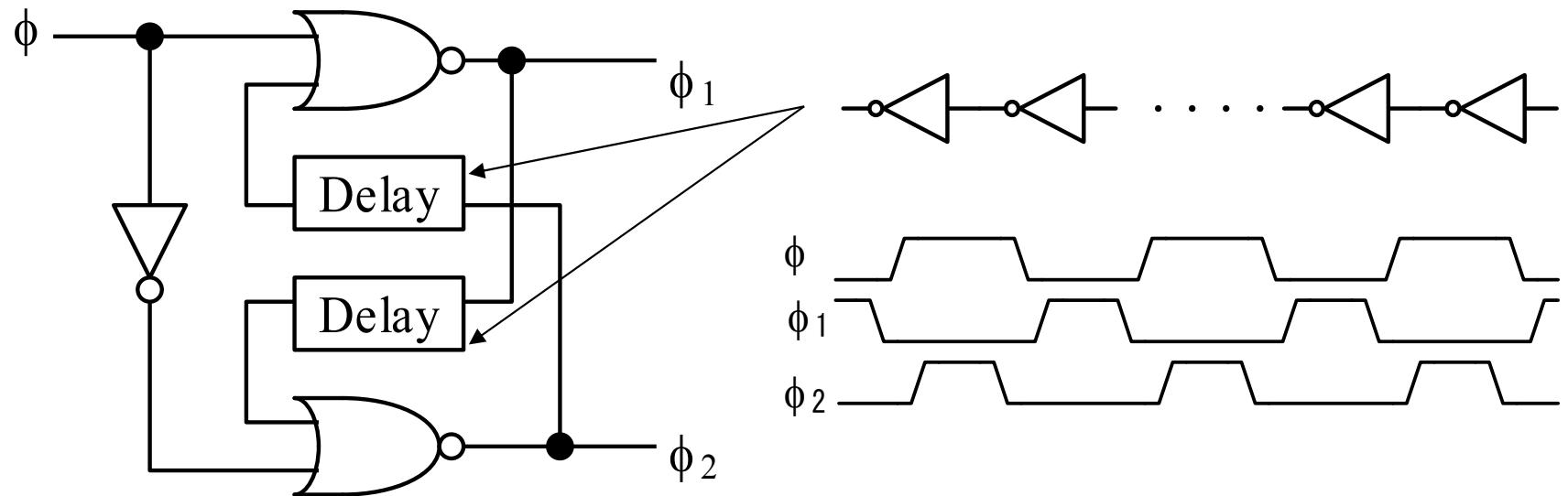


ϕ_1 ON OFF ON OFF

ϕ_2 OFF ON OFF ON

$t - \frac{T_S}{2}$ t $t + \frac{T_S}{2}$

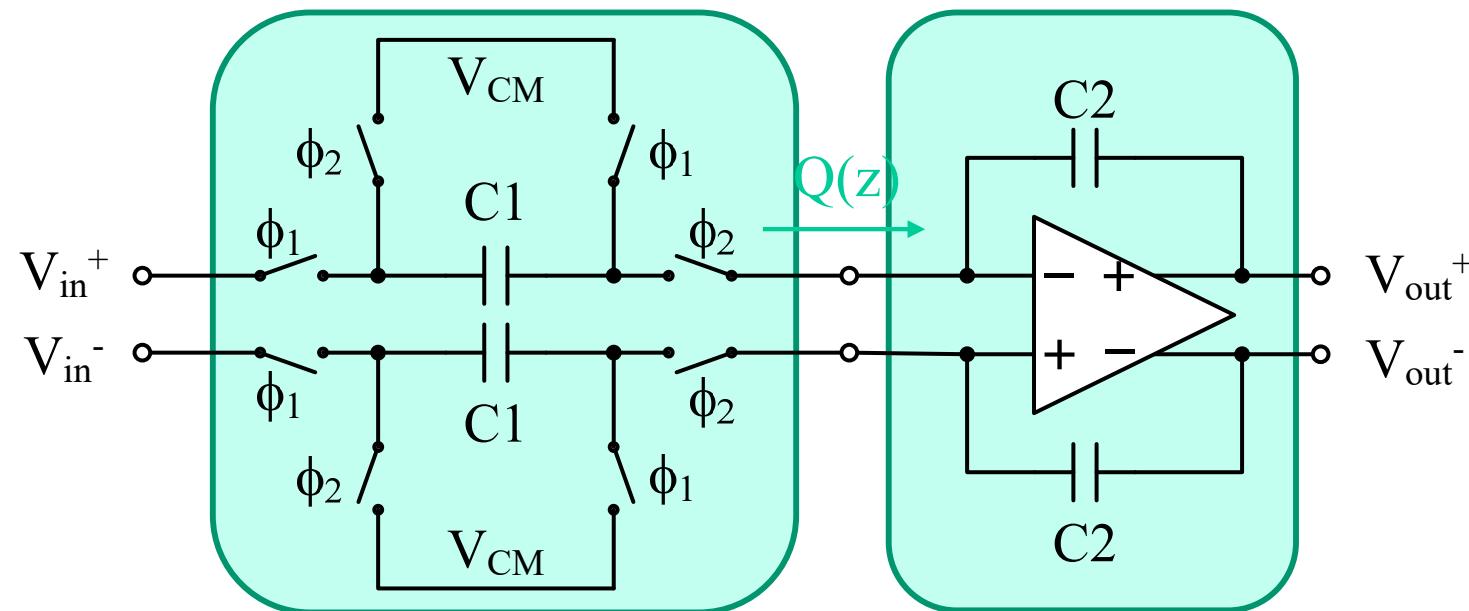
Non-overlapping clock generator



The two-phase clocks ϕ_1 and ϕ_2 are required to drive the switched capacitor. The edge of clocks ϕ_1 and ϕ_2 must not overlap, because the leak of the charge stored in capacitors causes the error of the signal processing.

DAI: discrete-time analog integrator 1

Positive phase integrator

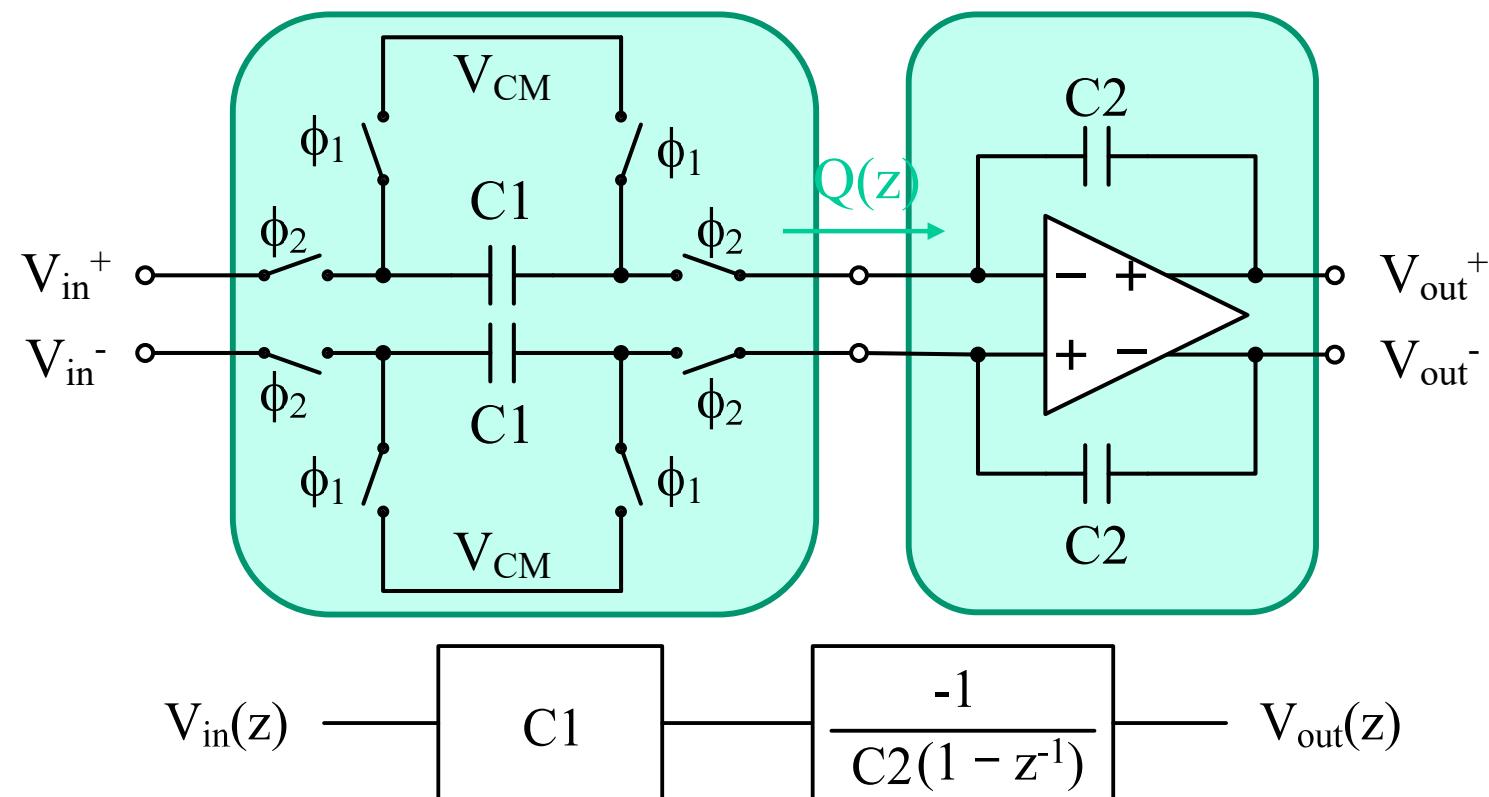


$$V_{in}(z) \rightarrow [-C1 \cdot z^{-1/2}] \rightarrow \frac{-1}{C2(1 - z^{-1})} \rightarrow V_{out}(z)$$

$$H(z) = \frac{C1}{C2} \frac{z^{-\frac{1}{2}}}{1 - z^{-1}}$$

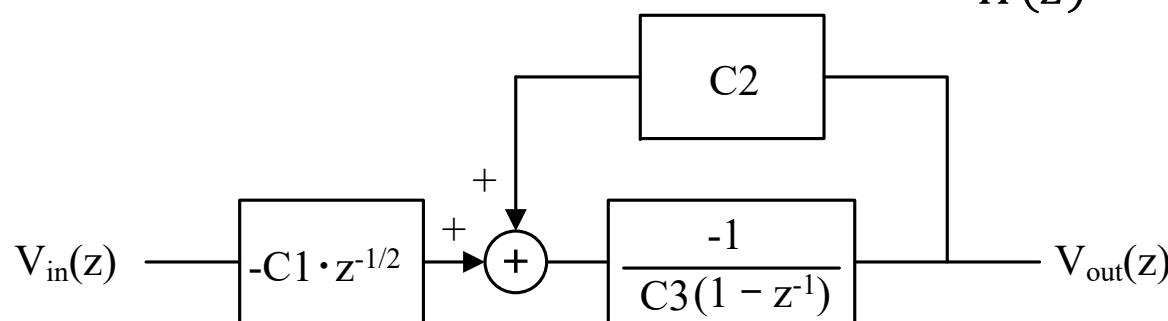
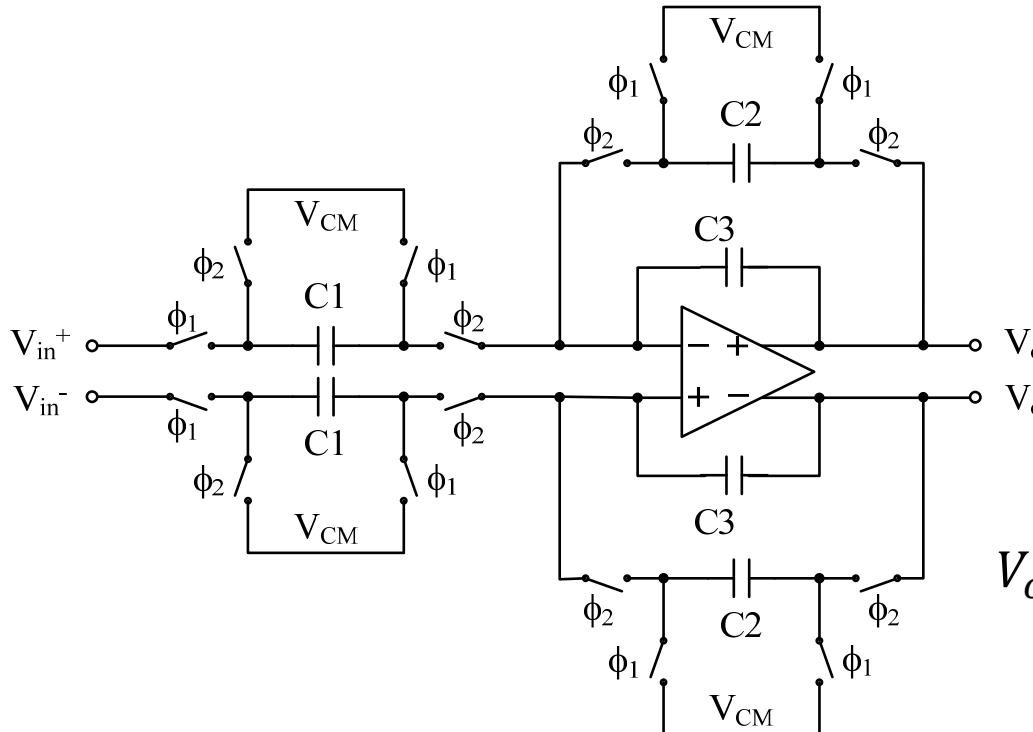
DAI: discrete-time analog integrator 2

Opposite phase integrator



$$H(z) = -\frac{C_1}{C_2} \frac{1}{1 - z^{-1}}$$

Implementation example

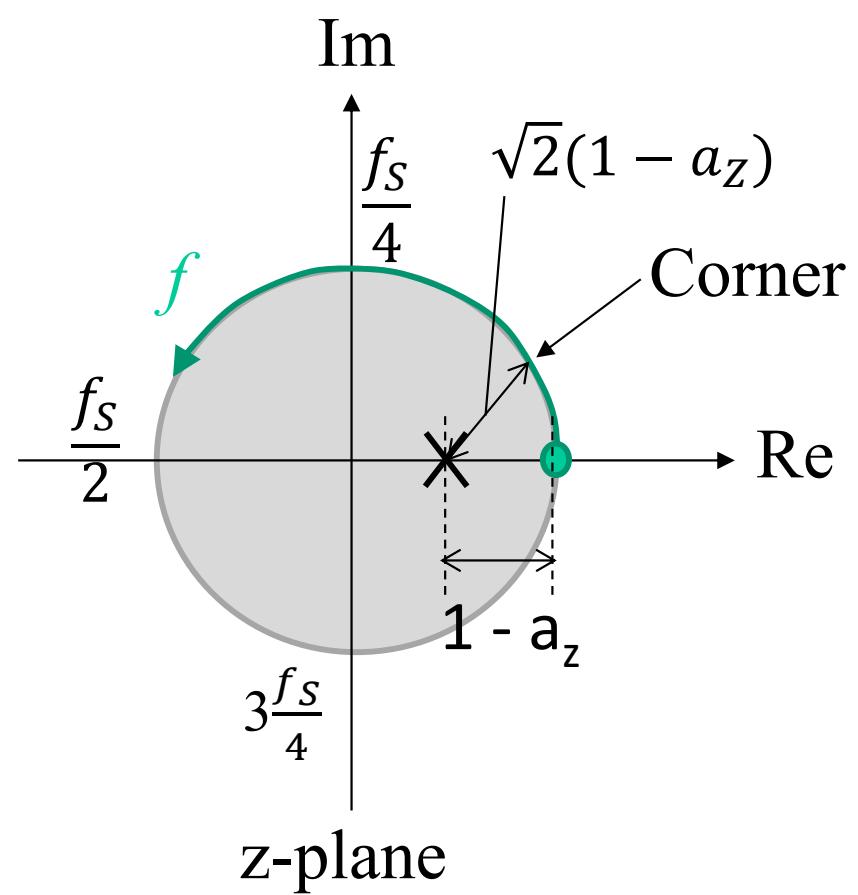
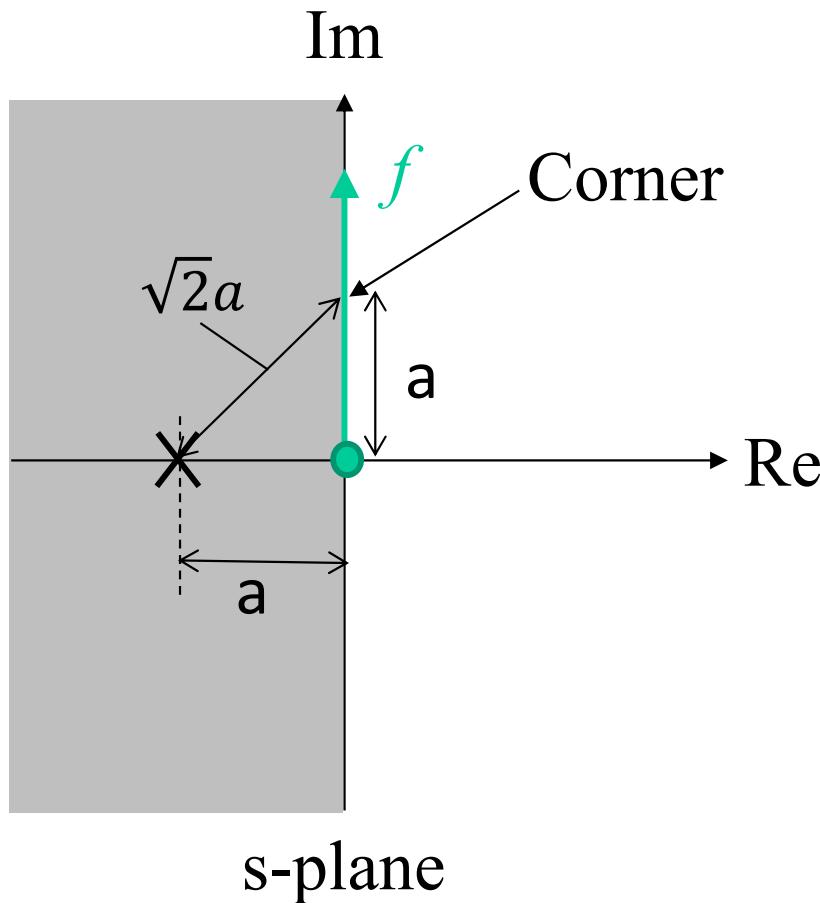


$$V_{out} = -\frac{1}{C3} \frac{1}{1 - z^{-1}} (-C1 z^{-\frac{1}{2}} V_{in} + C2 \cdot V_{out})$$

$$H(z) = \frac{V_{out}(z)}{V_{in}(z)} = -\frac{C1}{C2 + C3} \frac{z^{-\frac{1}{2}}}{z - \frac{C3}{C2 + C3}}$$

(LPF)

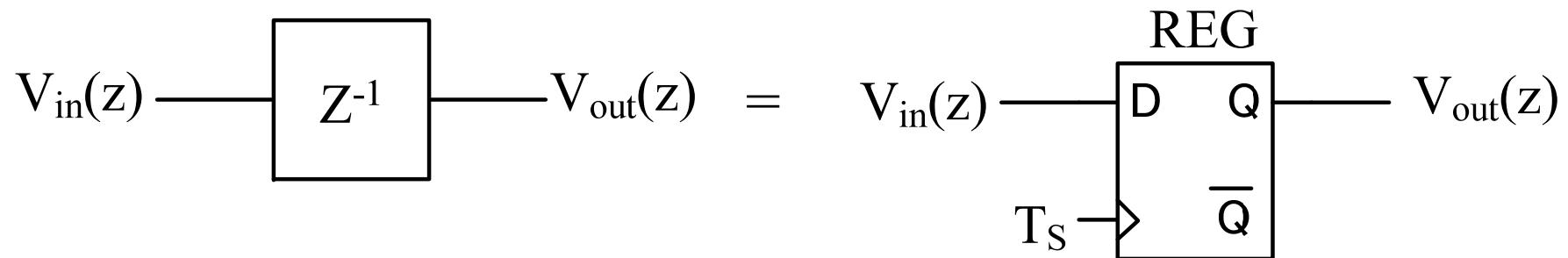
Poles in s-plane and z-plane



3.5 Digital implementation

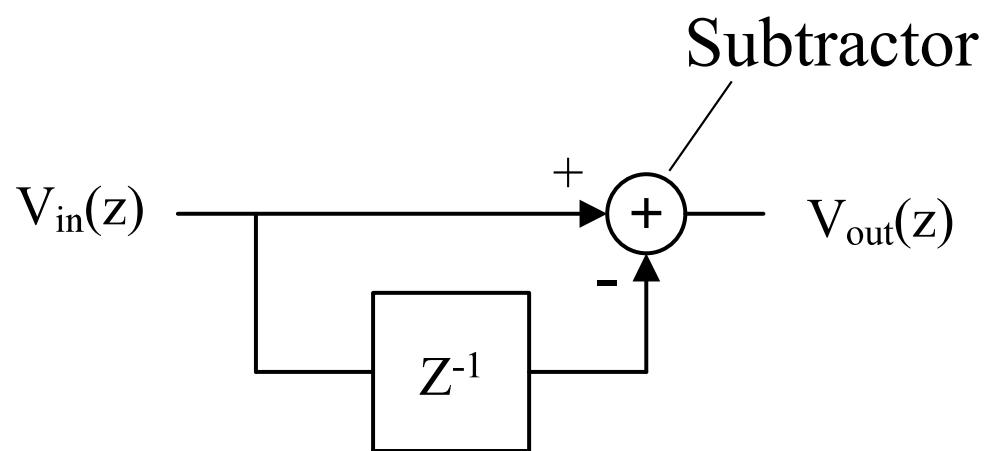
Digital operators 1

Delay

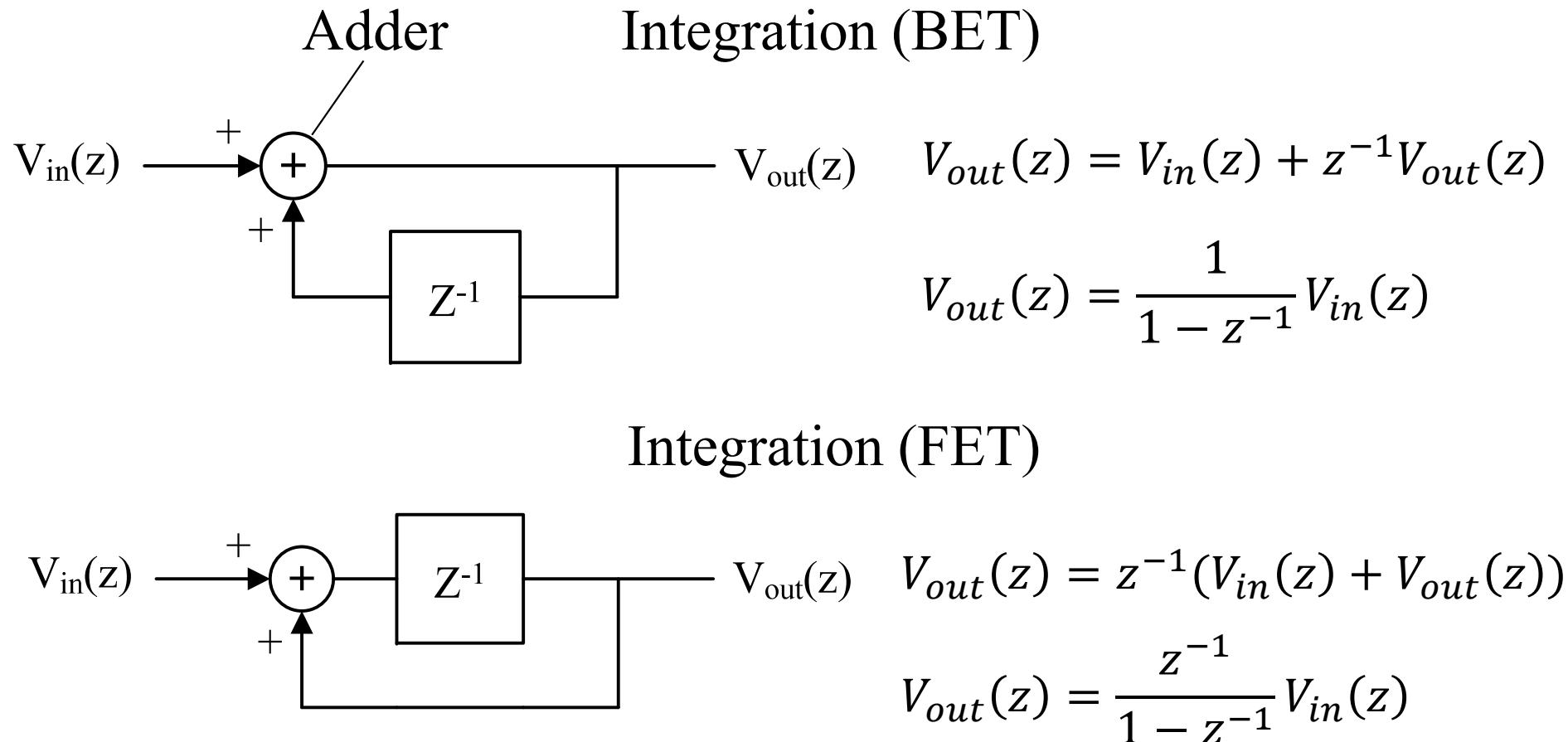


Differentiation (BET)

$$V_{out}(z) = (1 - z^{-1})V_{in}(z)$$

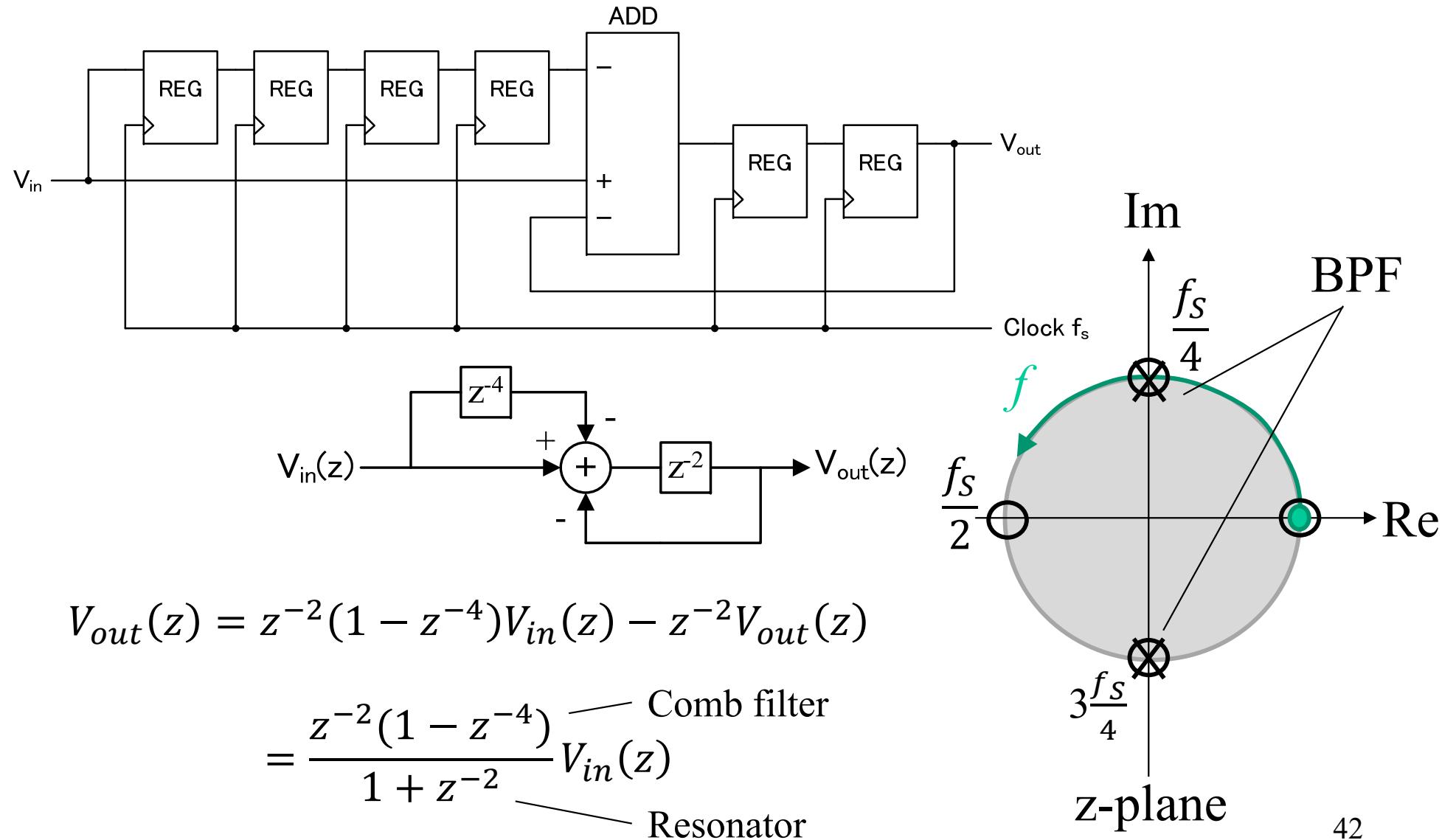


Digital operators 2



NOTE: The FET integrator does not output the hazards, because the digital delay element is the same as an register.

Implementation example



Automatic code generation and logic synthesis

Visit the following website.

<https://kitagawa.merl.jp/edu/index.php?MATLAB%20HDL%20CODER>

